

# HYDRAULIC INSTITUTE™

**PUMP TRAINING RESOURCES**  
BROUGHT TO YOU BY **PUMP SYSTEMS MATTER®**



## Pump System Assessment Course

# Pumping System Assessment

**FloFab**

**Instructor: Alex Kramer**

**Date: September 2018**

# Course Overview

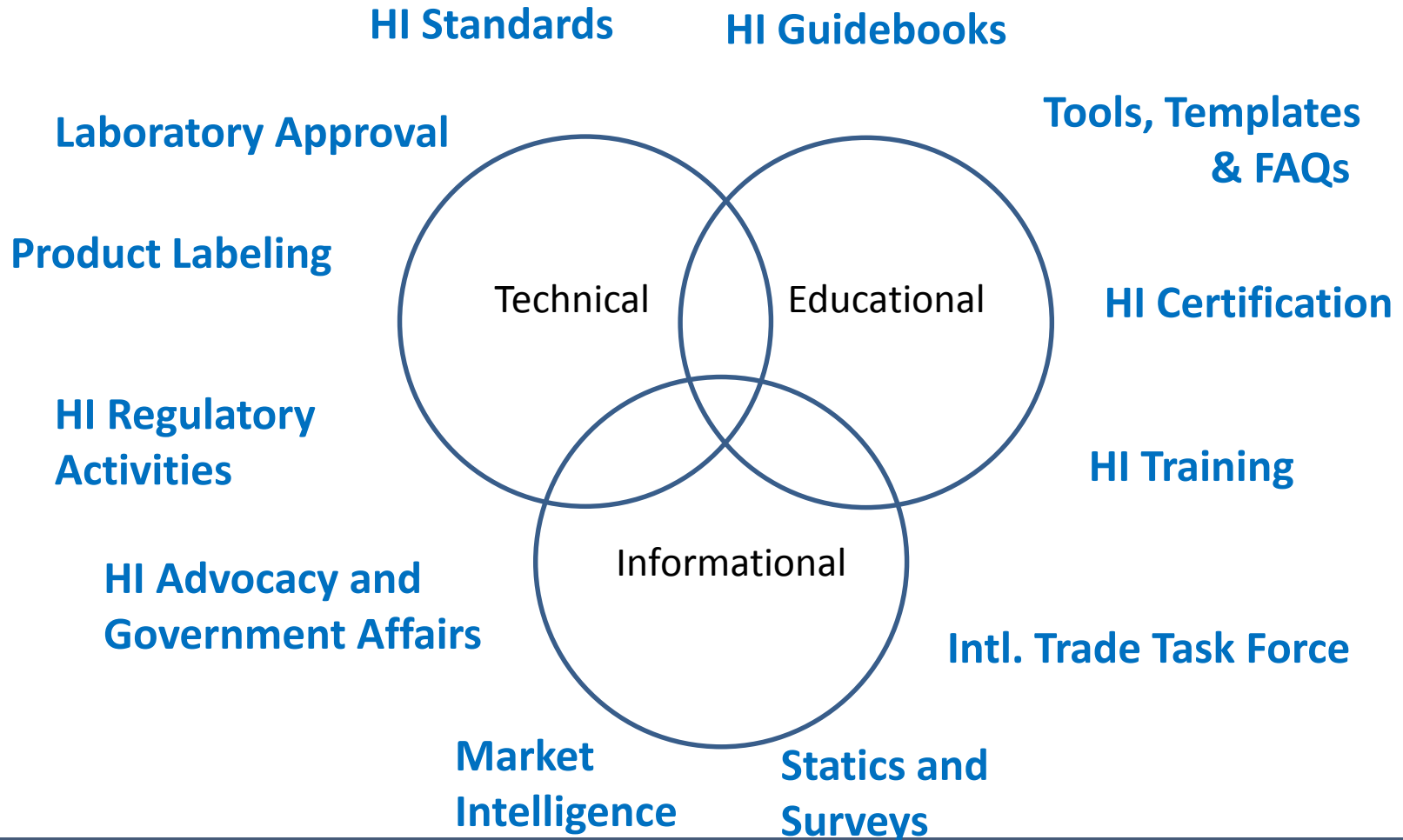
1. Pump World – 1-1/2hrs  
Hydraulic Institute  
Introduction to Pumping Systems
2. Water World – 1-1/2hrs  
Pump System Types in Commercial Buildings  
Examples
3. Flow Control & DHW – 1-1/2hrs  
Methods of Controlling Pumps  
Variable Frequency Drives  
Conclusions

# Hydraulic Institute and Pump Systems Matter

## Introduction

- **About the Hydraulic Institute:** The mission of the Hydraulic Institute is to be a value-adding resource to member companies, engineering consulting firms, and pump users worldwide by developing and delivering comprehensive industry standards, expanding knowledge by providing education and tools for the effective application, testing, installation, operation, maintenance, and performance optimization of pumps and pumping systems, and by serving as a forum for the exchange of industry information. For more information on the Hydraulic Institute, its member companies and its partners, visit [www.Pumps.org](http://www.Pumps.org)
- **Pump Systems Matter:** Established by the Hydraulic Institute, and leading utilities and energy efficiency organizations, PSM provides educational resources on the benefits to pump systems optimization and energy efficiency to improve bottom-line savings of end-user companies. PSM offers a robust schedule of webinars on pumps and pumping systems, based on HI standards and industry guidelines, and offers Pump Optimization course hosting opportunities to pump and supplier OEMs, pump distributors, energy efficiency organizations, water/wastewater utilities, electric power utilities and associations.

# HI Activities are Organized Around the Principle that Sound Technical Expertise will Educate and Inform...



# Educational Case Studies Working with Other Institutions: “Pump System Optimization” Case Studies

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## Process Pump Systems Optimization Study for a City Water Filtration Plant



### Pump Systems Challenges/Problems

- The following components and processes posed concerns:**
- Valves throttled to regulate flow rate, level, pressure, etc.
  - Employment of a bypass (recirculation) flow regulation
  - A batch process operated one or more pumps continuously
  - Frequent on/off pumping cycling in a continuous process
  - Cavitation noise, either at pump or within system
  - Equipment procurement policy based on lowest bid
  - A multiple parallel pump system changed in functionality
  - No flow, pressure or power indication

### Pump Systems Assessment: Data Collection Methodology and Results

- The pump systems assessment investigated:**
- Energy cost of operating pumping systems in their existing state
  - How pumps operated with respect to their best efficiency points
  - Potential energy savings strategies applicable to existing pumping systems
  - Cost of operating pumping system in optimized state

### Pump systems evaluation included:

- Identifying the most accurate pump representation with new pump curves based using field test data.
- Creating a system curve based on supplied isometric drawing
- Calculating energy consumption by determining existing pumping systems energy costs.
- Computing pump brake horsepower for the operating condition to determine motor load, motor efficiency, pump efficiency and energy consumption.
- Computing motor load to accurately calculate motor efficiency and energy consumption.
- Determining kilowatt requirements drawn by the motor-powered pumping system for a particular flow rate in calculating overall pump running costs.

### Facility Overview

Receiving a city directive to reduce costs (specifically with energy consumption, operations and maintenance), a water filtration plant conducted a pump systems assessment to evaluate the performance of its filtration pumps that were operating to optimum level.

These included:

- Plant water pumps
- Backwash pumps
- Surface pump
- Finish water pump system
- Reclaim water pump system

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## Chilled Water Pump Systems Optimization Study for a Data Center Facility



### Pump System Challenges/Problems

- The existing pump systems posed several concerns:**
- Faulty components and support equipment
  - Outdated building automation
  - Inefficient chilled water pump system operations
  - Lack of control over pump flow modulation of chilled water

### Pump Systems Assessment: Data Collection Methodology and Results

- A pump systems assessment investigated:**
- Installation of variable speed drives and new controls for chilled water pumping system and cooling units
  - Efficiency of operators of chillers in relation to chilled water pumps
  - Pump operating speeds
- Pump systems evaluation included:**
- Identifying the most accurate pump representation for chilled chillers and chilled water pumps
  - Identifying areas for equipment replacement that would be suitable for values.

### Facility Overview

A major data center facility consisting of 10,000 square feet of floor space. The facility is a multi-story building with a complex network of chilled water pipes, pumps, and chillers. The facility is located in a high-tech area and is used for data processing and storage.

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## Chilled Water Pump Systems Optimization Study for a Hospital



### Pump System Challenges/Problems

- The existing pump systems posed several concerns:**
- Flow higher than the design criteria caused resonance in the piping of the "old" part of the chilled water system.
  - Pumps operated on two different electrical buses. Electrical power to three pumps had a "soft" power factor at 0.82 while power supplied to two pumps had a power factor of 0.85.
  - Two pumps were configured with custom variable frequency drives (VFD) while the others were specified with NEMA P/NB starters.
  - One pump tripped an overload after operating for an hour while another tripped an overload after just 10 minutes. One pump operated continuously. Operation in the overload protection system probably caused differences in pump run time.
  - With two pumps running VFD versus at 50Hz, which yielded 11.1:1:24 on the motor. With one pump operating and the last one in VFD-overrun pump, the VFD drove the motor to 62Hz.
  - Water for cover an section was located 12 inches from piping while original clearance was noted at 3.35".

### Pump Systems Assessment: Data Collection Methodology and Results

- A pump systems assessment investigated:**
- Why motors draw high amperage (in service factor)
  - Why pumps operated differently
  - How pumps operated with respect to their Best Efficiency Points (BEP)

### Pump systems evaluation included:

- Identifying the most accurate pump representation with new pump curves based on the field test data. The original pump curve supplied by the customer (over two decades ago) had a design speed of 1750 rpm. Due to the increased operating pump speed and the fact a certified performance curve was not obtained when installing new pumps, plotting a new curve was mandatory.
- Creating a system curve to determine the pump operating point.

### Facility Overview

A large hospital performed a pump systems optimization study on a chilled water system used for plant processes and HVAC loads to identify areas for improved efficiency and reliability. The chilled water system consisted of five water pumps, two of which were newly installed to add chill water loads for a proprietary section of the piping system. While the new pumps operated at 100% efficiency, existing pumps ran at 60% efficiency. The system also was controlled manually, even though variable frequency drives were in auto mode.

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## Pump and Motor Optimization Study for a Beverage Bottling Plant



### Pump System Challenges/Problems

A beverage bottling plant experienced performance problems with a pasteurizing system composed of 16 pumps ranging from 10HP to 20HP that were driven by custom-built motors. A pump and motor optimization study was conducted to identify the cause of bearing failures that resulted in high vibration levels. Three motor (15HP and 20HP) failures and tipping of another motor due to overloads.

### Facility Overview

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## Pivot Irrigation Pump Systems Optimization for Agriculture



### Pump System Challenges/Problems

- The existing pump systems posed several concerns:**
- The center irrigation system was highly inefficient, without a centralized approach to manage and control water flow to all corn and soybean fields over large tracks of land.
  - To maintain and operate the existing irrigation system required 7000 man hours annually.
  - The farm needed to save water annually to obtain energy savings relative from a local utility provider.
  - Conserving 300 acres of land of flood irrigated land to a center pivot irrigation required removal of old water control, dikes and barns and the addition of new water and electrical lines.

### Pump Systems Assessment: Data Collection Methodology and Results

- A pump systems assessment investigated:**
- Overized pumps with piping allows too close to the pump
  - Pumps with cavitation and high vibration problems causing bearing and shaft failure in the pumps and motors
  - Alignment between motors and pumps that did not meet Hydraulic Institute standards
  - Lack of pressure gauges on pumps
  - Maintenance costs as OEM life expectations for bearings and wear rings did not match specifications

### Pump systems evaluation included:

- Identifying the most accurate pump representation using new pump curves generated with field test data
- Creating a system curve with new operating data to determine the pump operating point
- Pipe flow analysis and modeling to simulate system components and their interaction to gain a greater understanding of existing irrigation system and validate field data and system fluid dynamic behavior.

### Facility Overview

A first-generation, 500-acre farm located in Western Ohio, that raises corn and soybean was upgrading its existing floor irrigation and pumping to increase energy and labor savings while gaining greater control over operations. Under consideration was a center pivot irrigation and water system controlled from a single location with a 250HP pump that drew water from local rivers and groundwater. A pump systems optimization study was performed to review existing irrigation system, specifications for the proposed upgrade and recommend a simple, yet high-tech system that would maximize energy, water and labor savings.

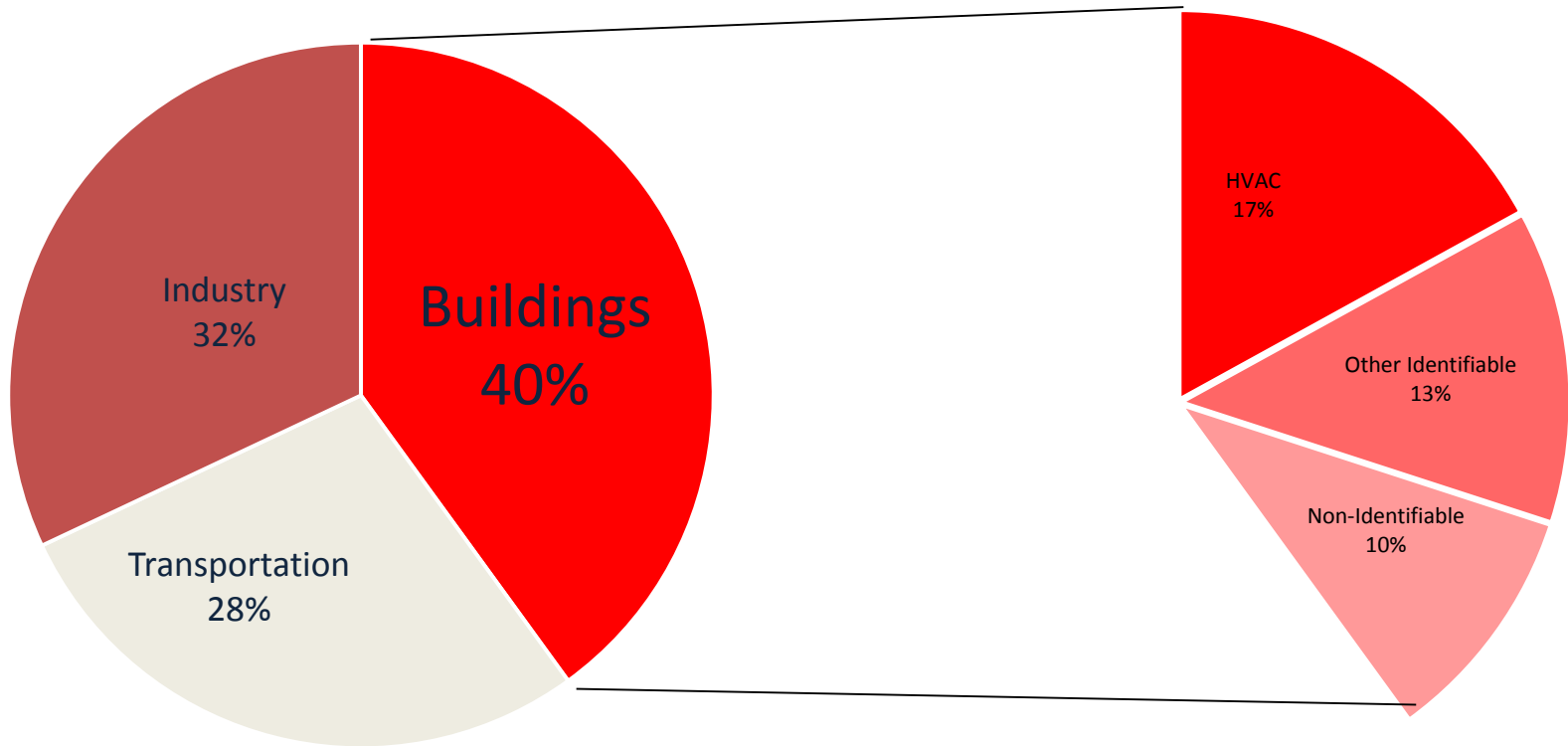
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# Pump World

# Use Energy Consumption

Total US Energy Consumption

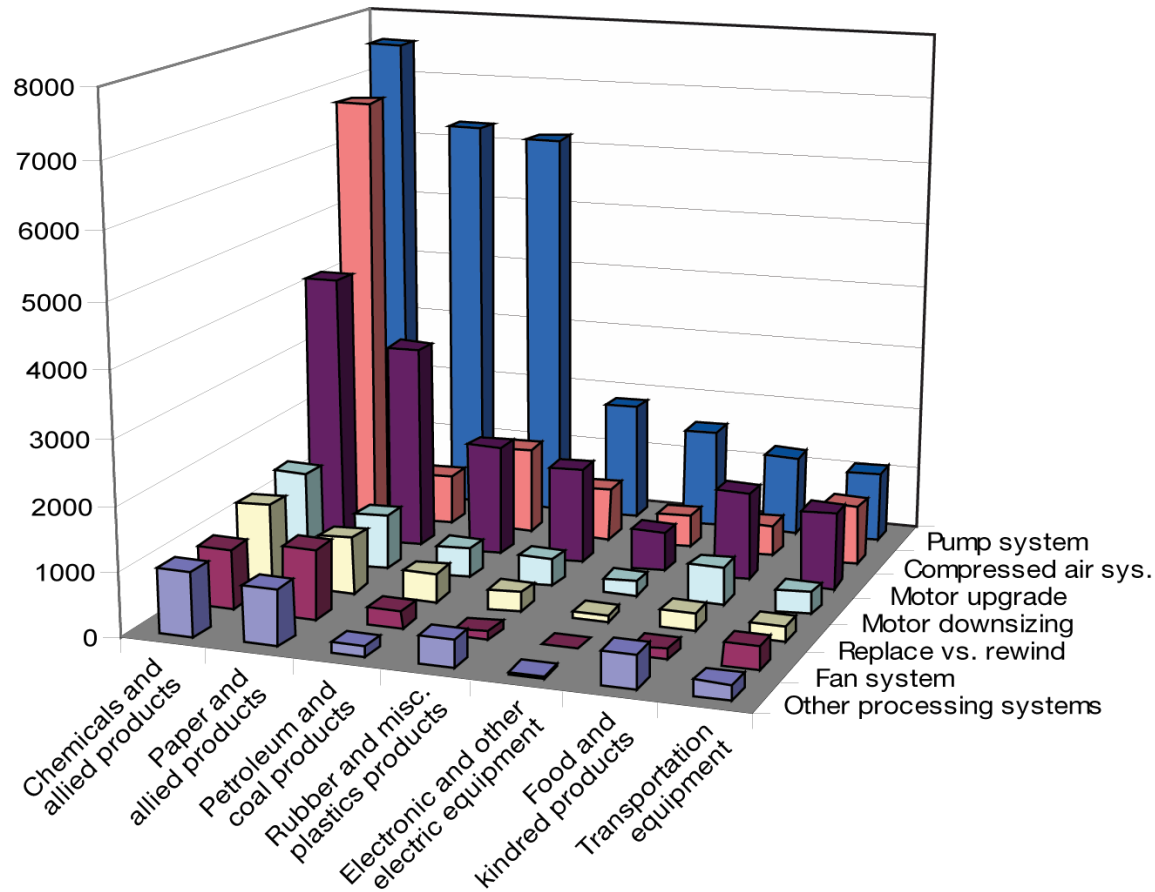
US Building Energy Consumption



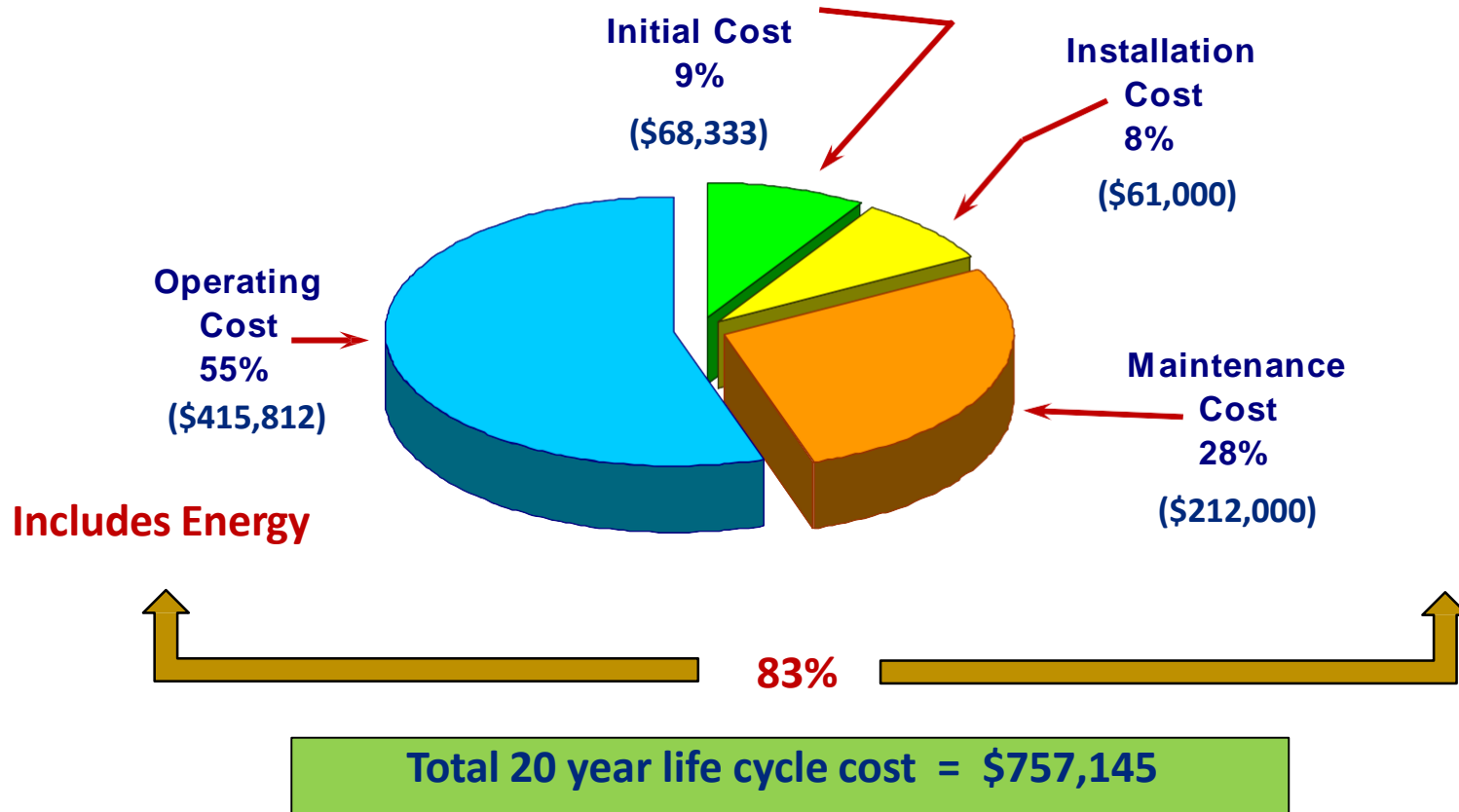
Source: US Department of Energy – Buildings Energy Data Book (2010)



# Pump Systems Have Greatest Energy-Saving Potential Across All Industries



# 20 Year Life Cycle Cost of Conventional 75HP Pumping System



# Initial Costs are the Wrong Focus

## Example: Lifetime Energy Costs of a Motor

Purchase Price

**\$5,000**

Installed

**\$20,000**



Energy Cost

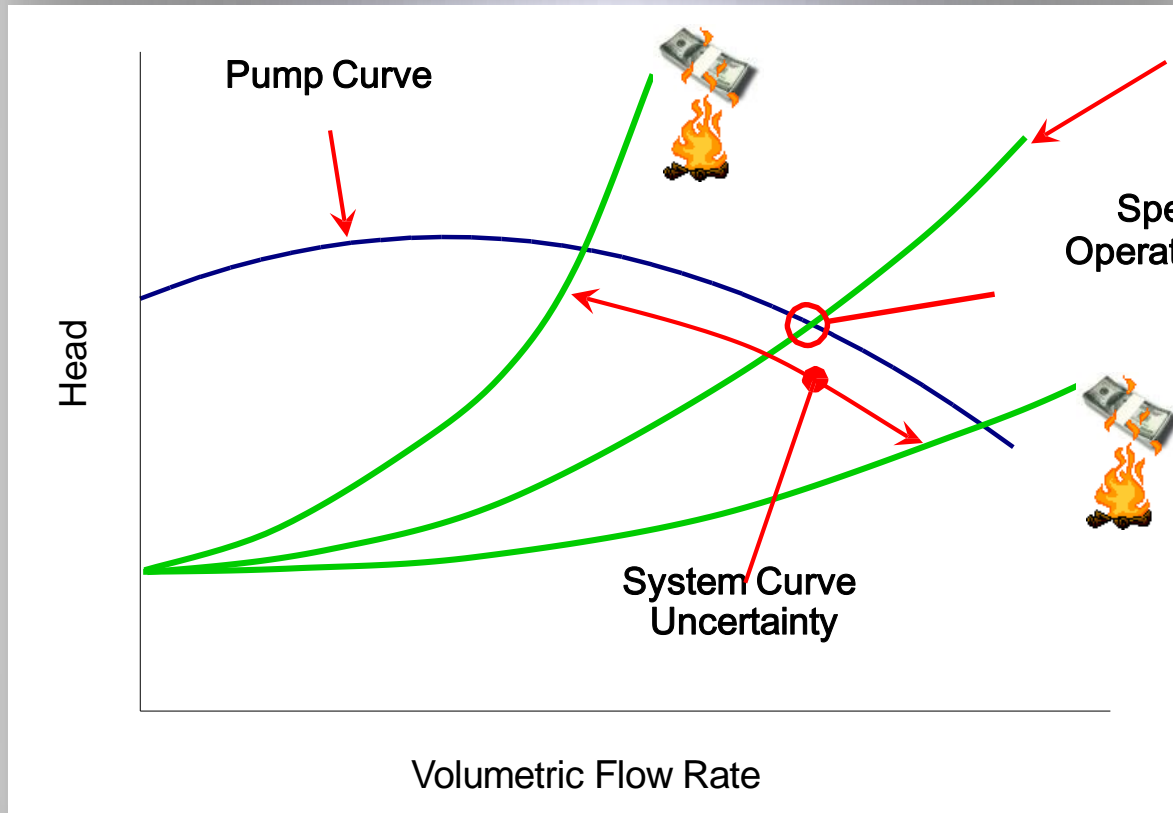
**\$810,000**

**(162 X Purchase)  
(40 x Installed)**

**Example:** 100 HP motor @ \$0.08/kWh electricity (\$54K/yr) 24/7 for 15-yr life

# Key Concept

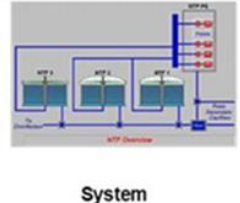
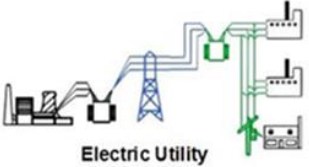
System Curve  
(as Specified)



# Key Points

- Most pump systems are oversized
- Look beyond energy savings,
- Evaluate the entire system,
- Life time energy cost is a major cost compared to first cost

# Think System



Energy Efficiency Improvements

**Component Optimization** involves segregating components and analyzing in isolation.

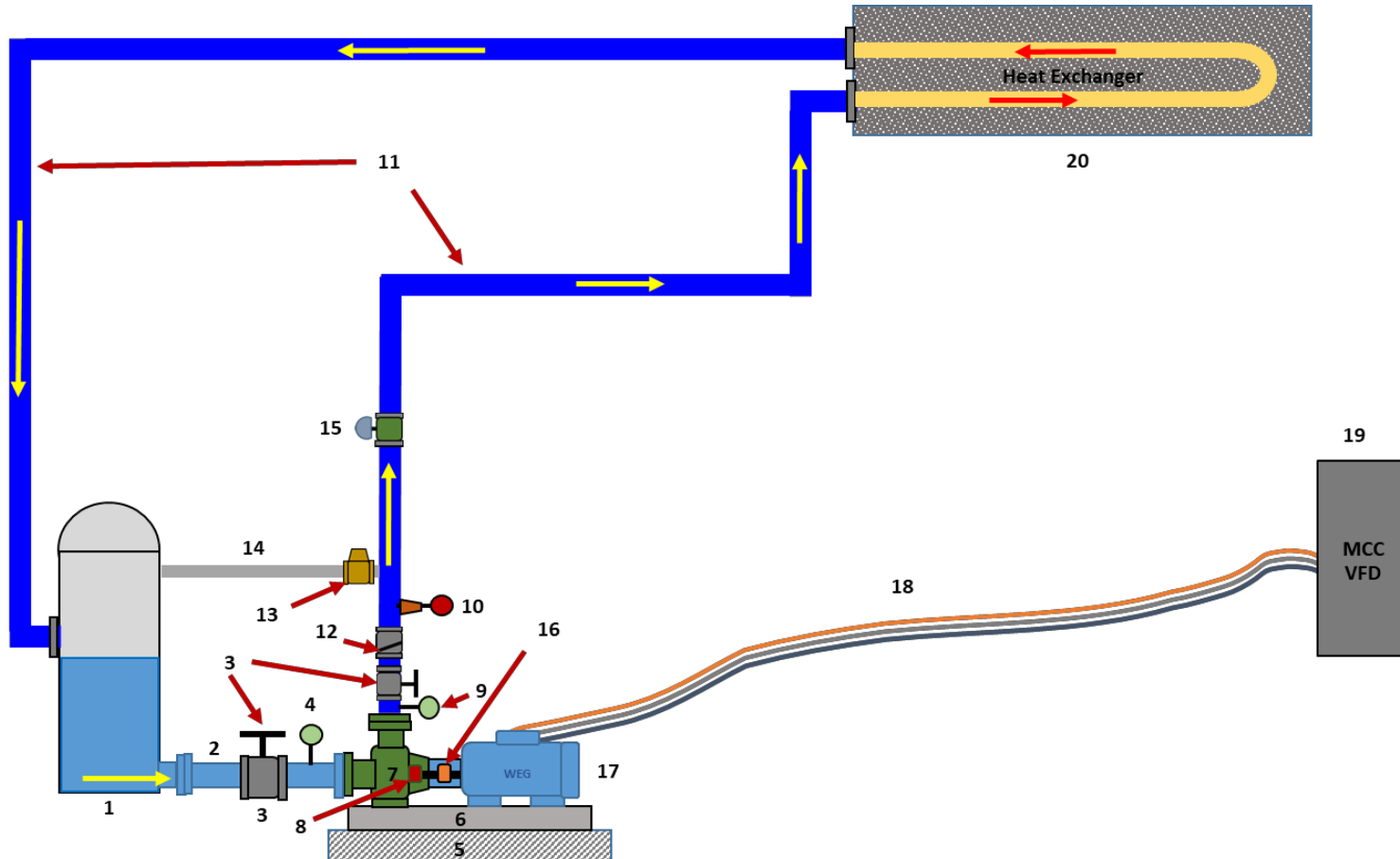
**System Optimization** involves looking at how the whole group functions together and how changing one can help improve the value of the entire application solution.

At each interface, there are inefficiencies. The primary objective should be to maximize the overall cost effectiveness of the entire system, or simply stated... "how much output energy is delivered per unit of input energy."

# Look at Entire System to Save Energy

<b>Process Requirements</b>	Flow required Head required	17200 gpm 200 feet	17200 gpm 150 feet	17200 gpm 200 feet	17200 gpm 200 feet
<b>Piping elements</b>	Additional system friction loss	50 ft	0 ft	50 ft	55 ft
<b>Component Efficiencies</b>	Motor eff	94%	94%	94%	96%
	VFD efficiency factor	100%	98%	100%	100%
	Mechanical drive eff	100%	100%	100%	100%
	Pump eff	65%	88%	70%	65%
<b>Electrical</b>	Energy cost per kWh	\$0.05	\$0.05	\$0.05	\$0.05
	Operating hours per year	6250	6250	6250	6250
	Factor	Base	Reduce friction by 50 feet.	Increase pump efficiency by 5 points.	Increase motor efficiency by 2 points.
<b>Output</b>	System efficiency	49%	81%	53%	49%
	System input power required for process	1421.7 bhp	803.7 bhp	1320.2 bhp	1392.1 bhp
	Power required for additional friction	355.4 bhp	0.0 bhp	330.0 bhp	382.8 bhp
	Total power required	1777.2 bhp	803.7 bhp	1650.2 bhp	1775.0 bhp
	Total cost per year	\$414,306	\$187,360	\$384,712	\$413,788
	Cost Savings		\$226,946	\$29,593	\$518
1	2	A	B	C	D

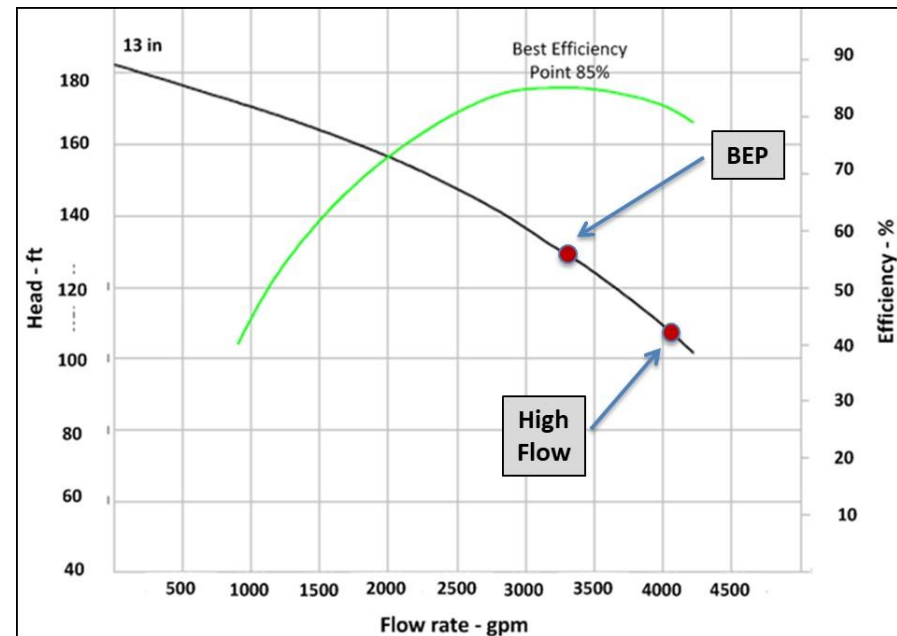
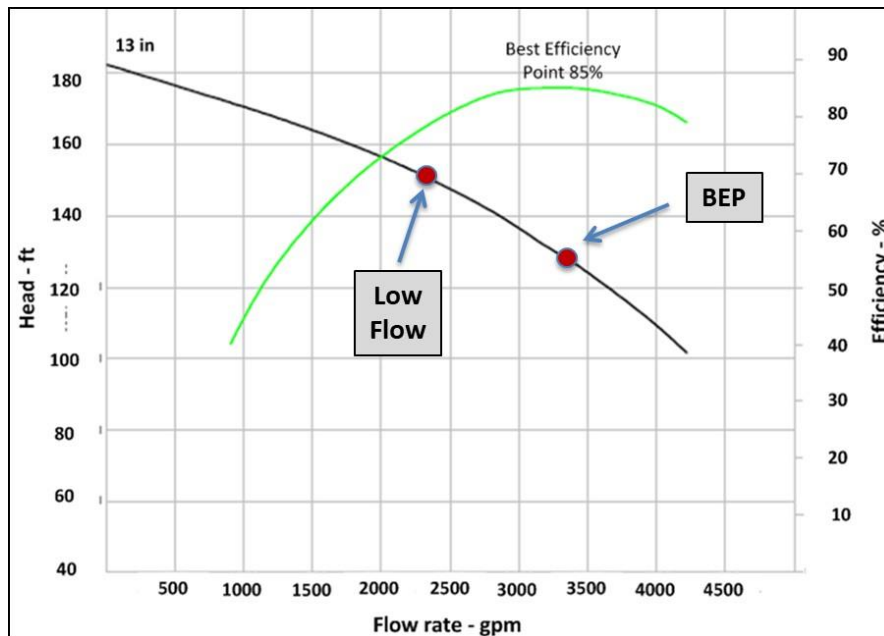
# Typical Pump System Components





# Centrifugal Pump Facts

Centrifugal pumps should be selected and normally operated at or near the manufacturer's design rated conditions of head and flow.



# The System: What is a System Curve?

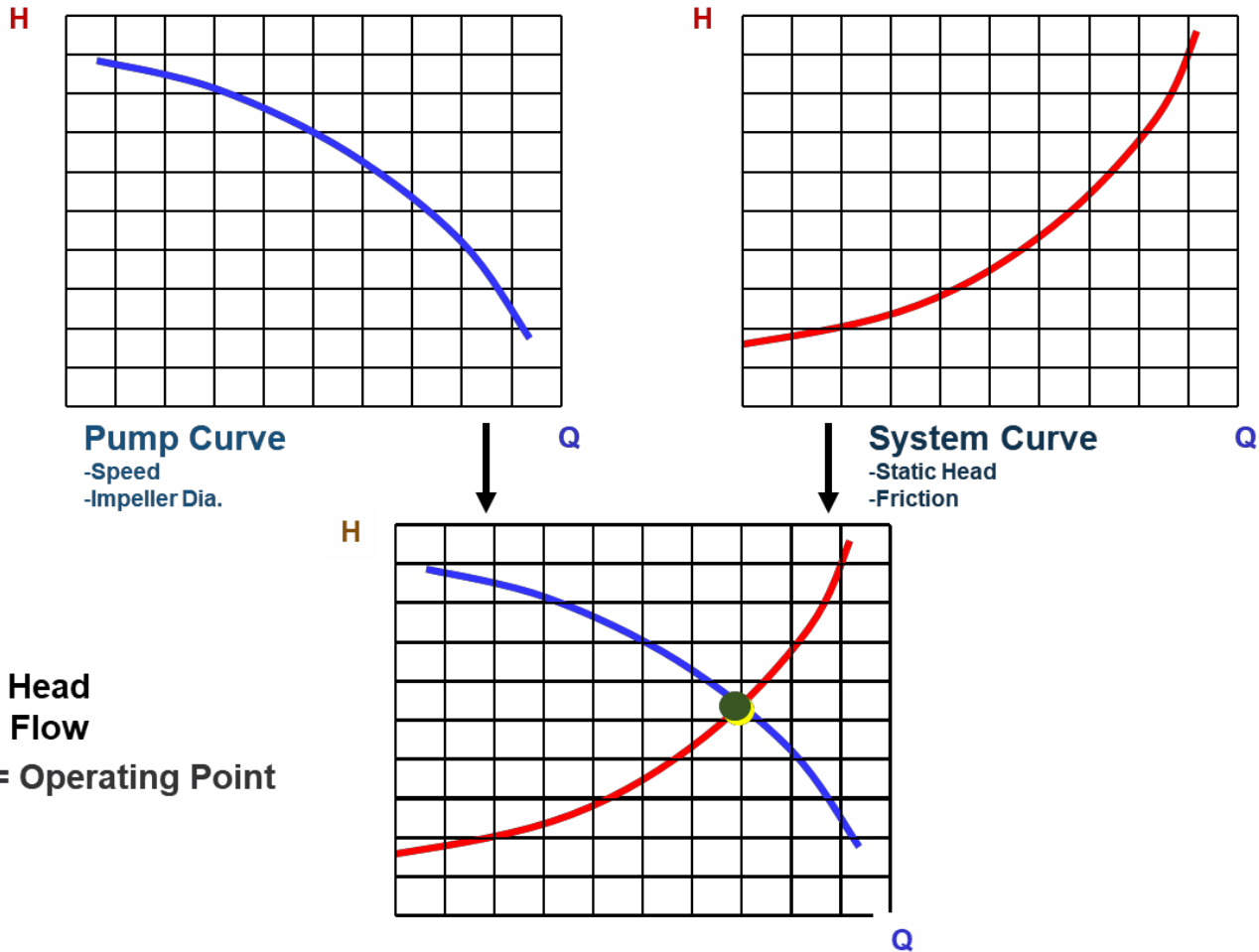
A system curve represents the sum of the static head and the friction loss due to flow of fluid through a system.

The pumping system will operate where the pump and system curves intersect

System curves help demonstrate pumping system behavior in a graphical manner

If a system curve can be determined, it can help identify the effects of pump and/or system modifications

# System Curve



# System Optimization and Improvement Opportunities

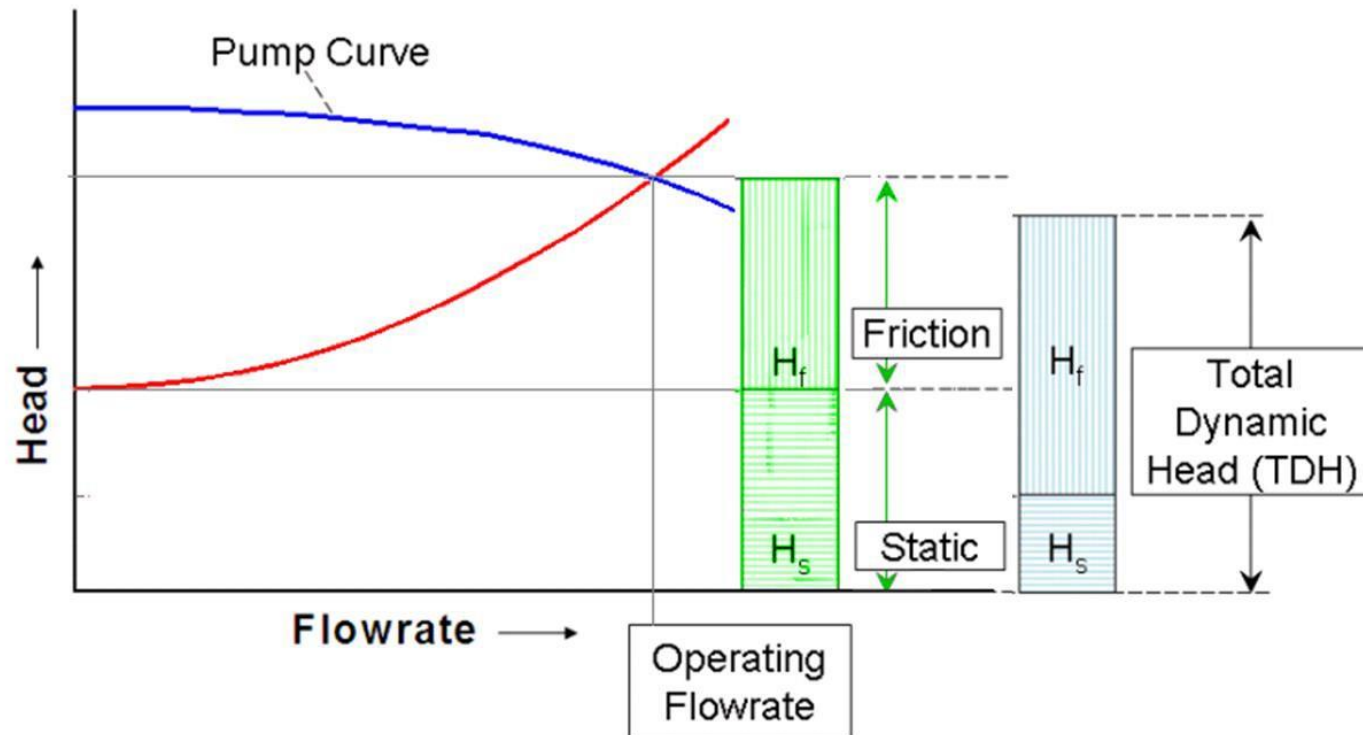
- Eliminate unnecessary uses
- Improve Operations & Maintenance (O&M) practices
- Improve piping configuration
- Consider alternative pump configurations
- **Change pump speed**

# More System Optimization Opportunities

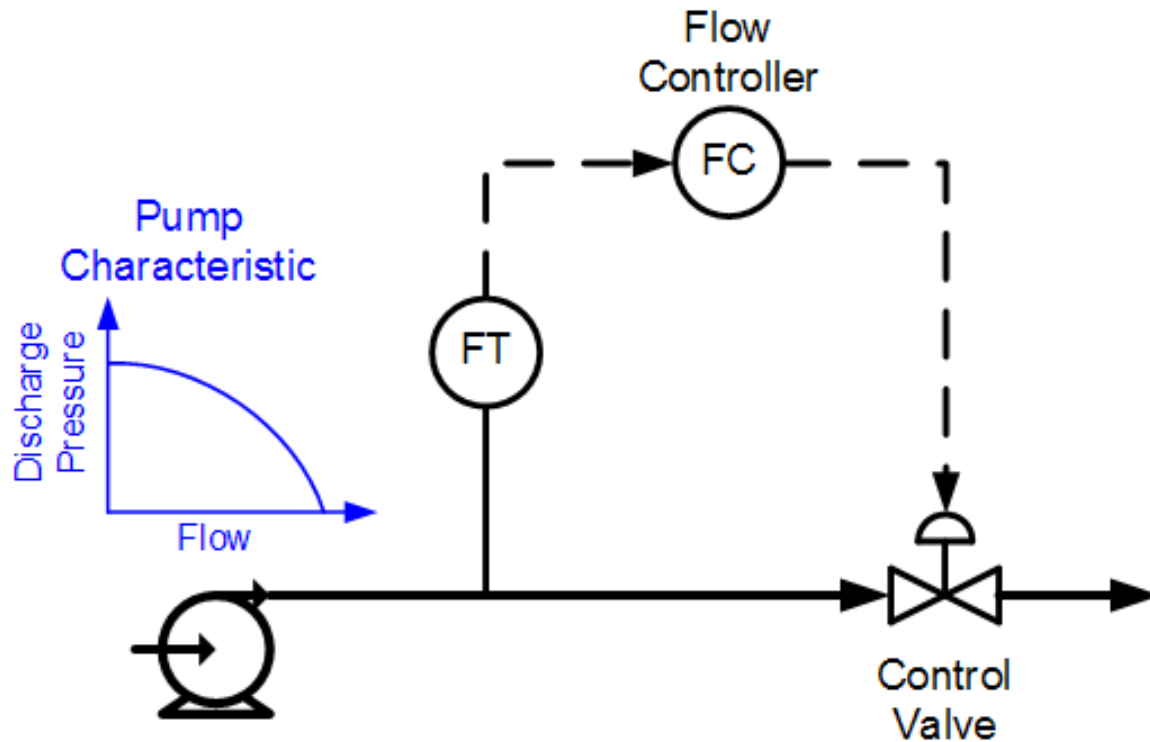
- Using a pump when the fluid is not needed
- Running two pumps when only one is needed
- Continuing to run pumps in a batch-type process when products are not being produced
- Excessive pump head or flow

# Friction in Pump Systems

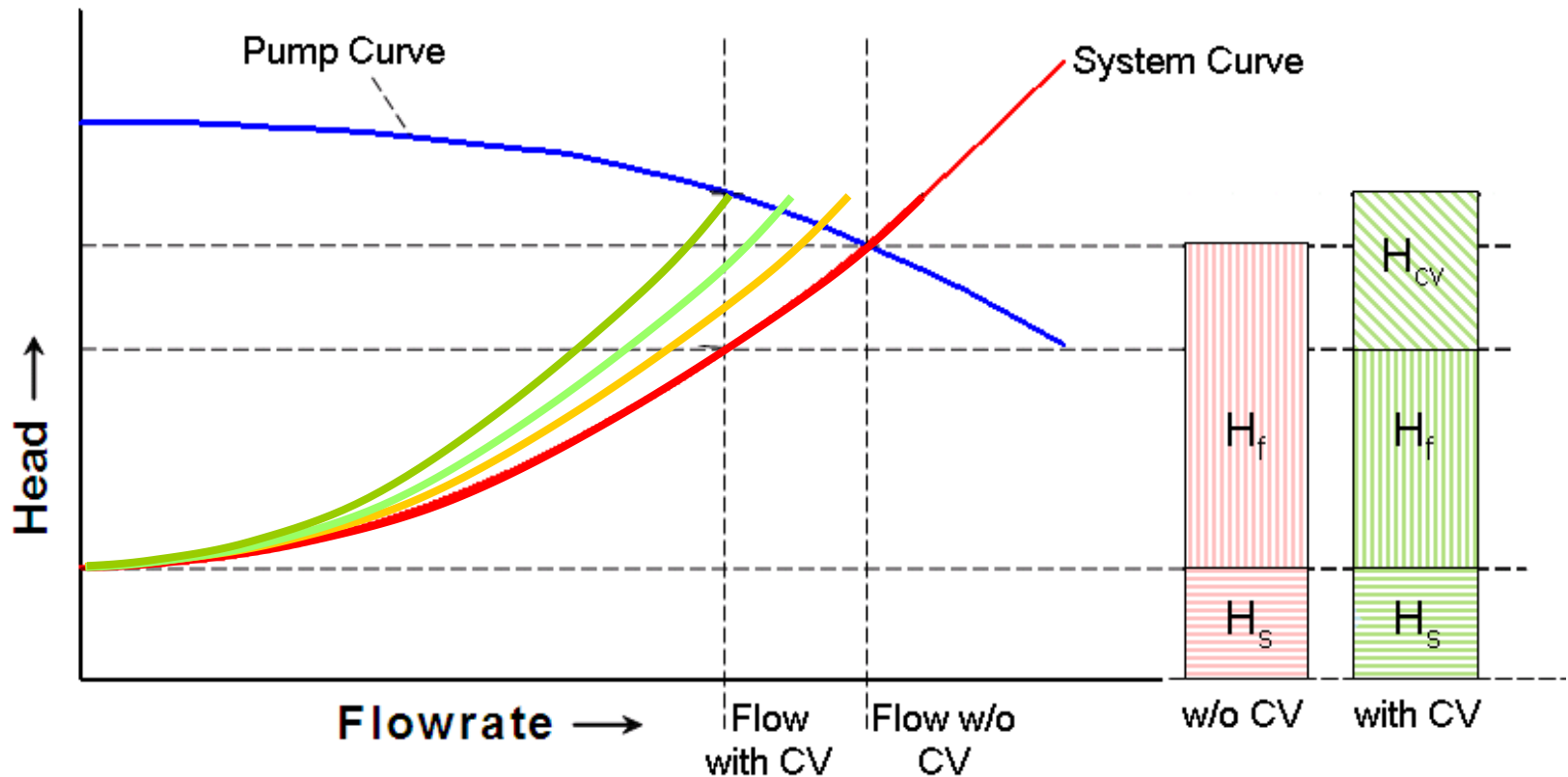
- Friction occurs in pump systems due to **irrecoverable** hydraulic losses
- Friction is also used to control flow or pressure, **recoverable hydraulic losses**



# Throttling Valves and Friction

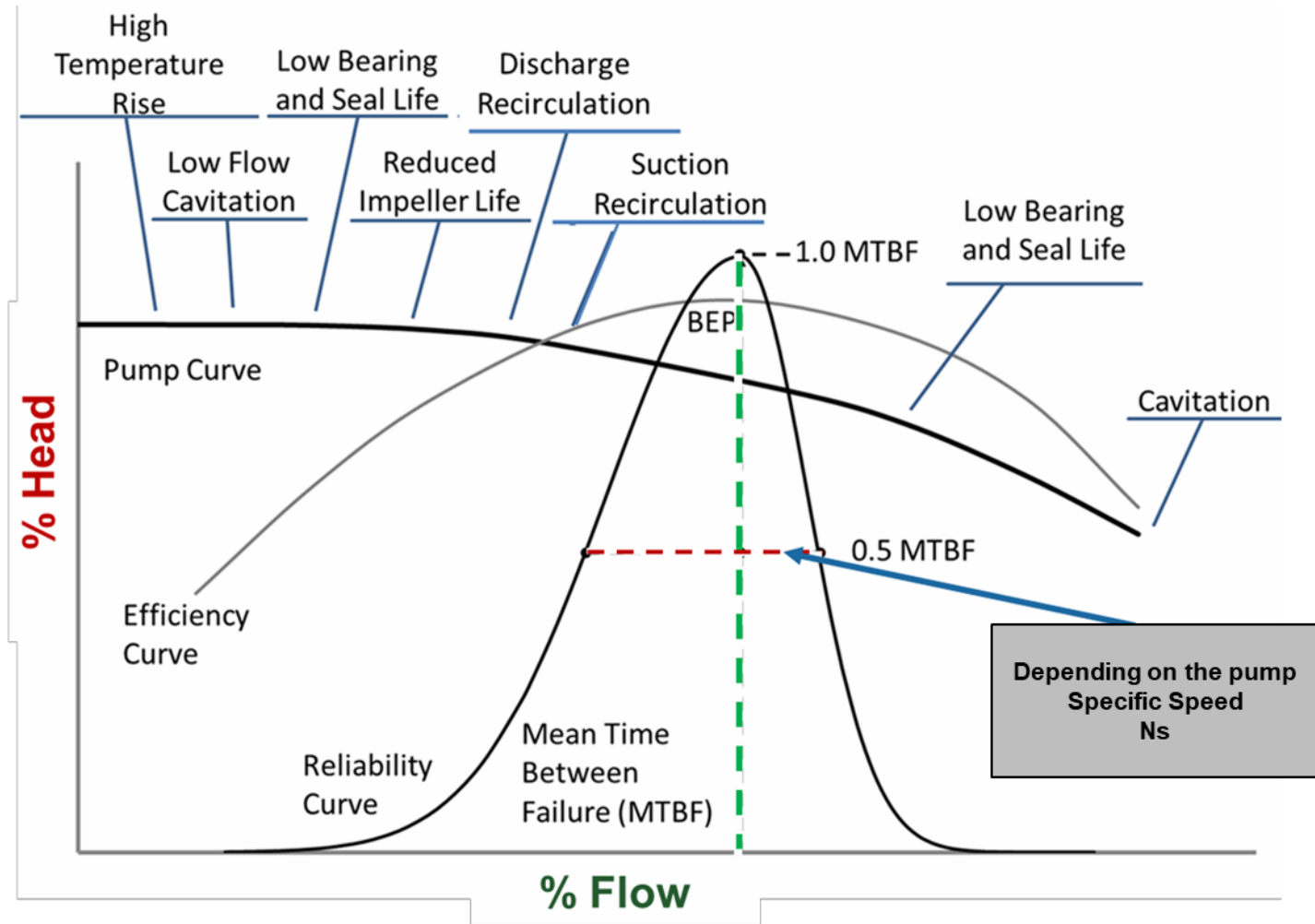


# Effects of a Control/Throttling Valve

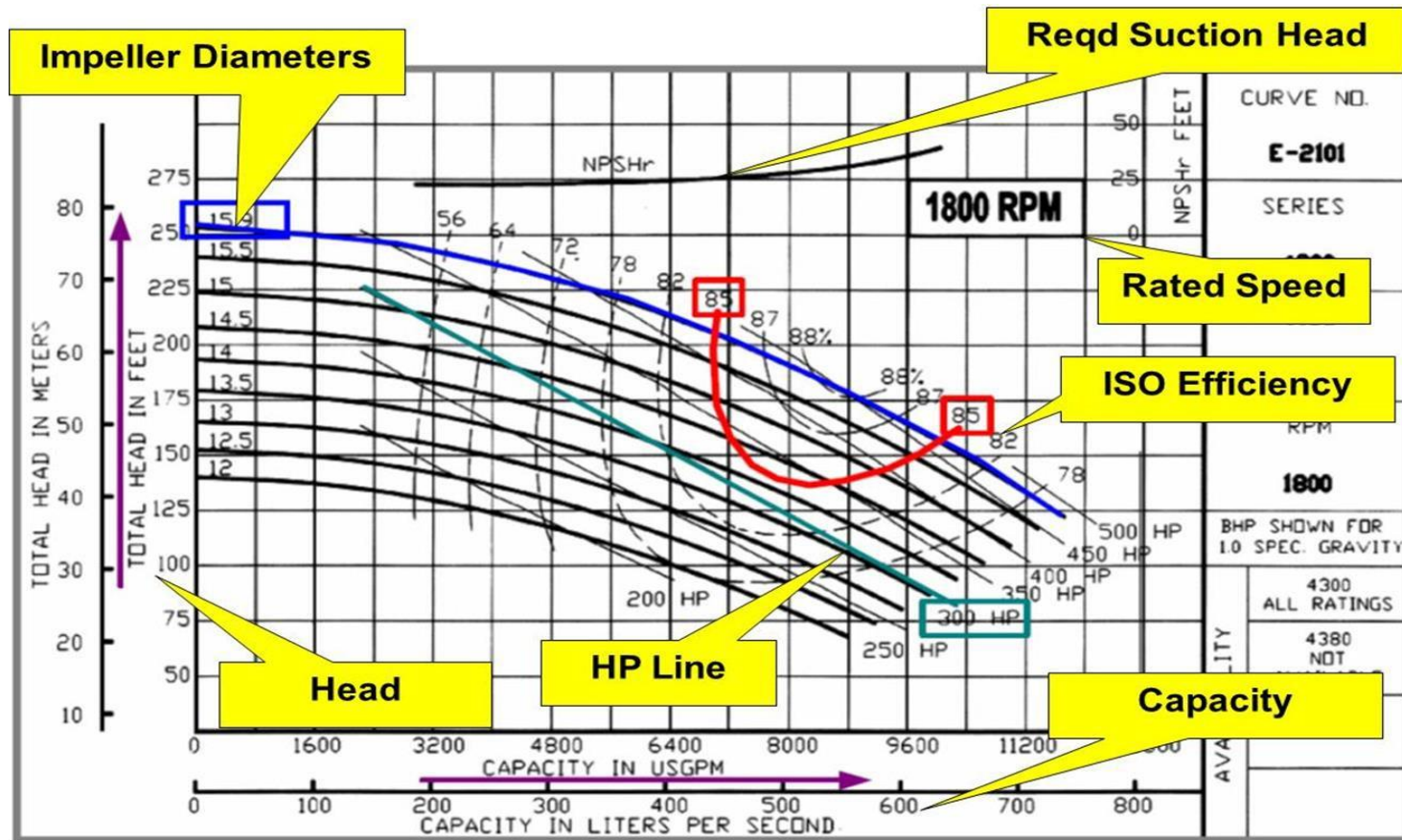




# Pump Reliability and BEP



# Data for Specific Area of Pump Curve



# Pump Affinity Rules

Speed

$$\left( \frac{Q_1}{Q_2} \right) = \left( \frac{N_1}{N_2} \right)^1$$

$$\left( \frac{H_1}{H_2} \right) = \left( \frac{N_1}{N_2} \right)^2$$

$$\left( \frac{P_1}{P_2} \right) = \left( \frac{N_1}{N_2} \right)^3$$

Diameter

$$\left( \frac{Q_1}{Q_2} \right) = \left( \frac{D_1}{D_2} \right)^1$$

$$\left( \frac{H_1}{H_2} \right) = \left( \frac{D_1}{D_2} \right)^2$$

$$\left( \frac{P_1}{P_2} \right) = \left( \frac{D_1}{D_2} \right)^3$$

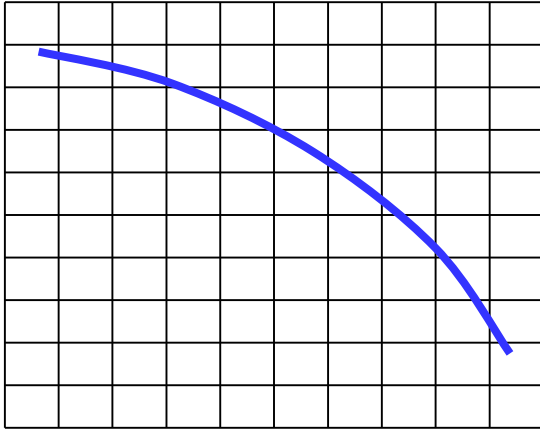
**Q = flow rate**   **H = head**   **P = power**  
**N = speed**                      **D = diameter**

# Pump Affinity Rules

Speed	Volume	Pressure/ Head	Horsepower Required
100%	100%	100%	100%
90%	90%	81%	73%
80%	80%	64%	51%
70%	70%	49%	34%
60%	60%	36%	22%
50%	50%	25%	13%
40%	40%	16%	6%
30%	30%	9%	3%

# Pump and System Curves

H

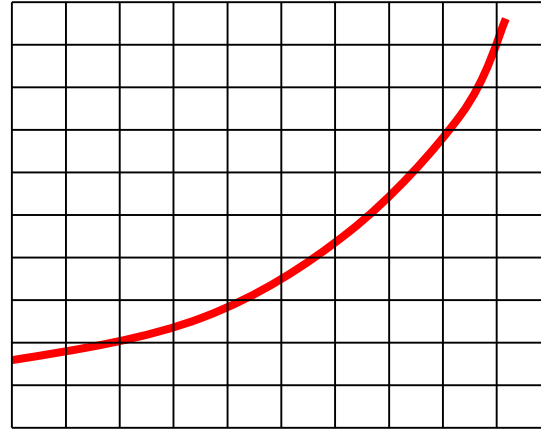


**Pump Curve**

-Speed  
-Impeller Dia.

Q

H

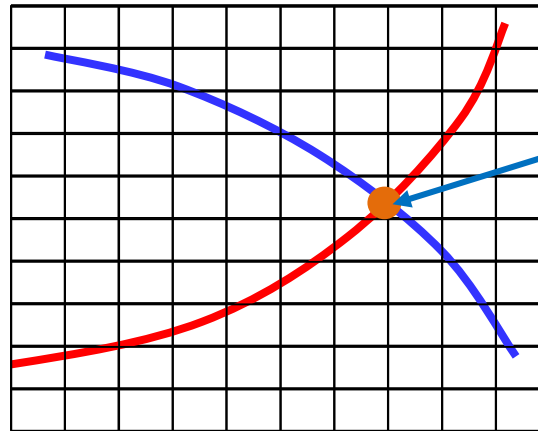


**System Curve**

-Static Head  
-Friction

Q

H



Q

For fixed speed pumps, the operating point is located at the intersection of the pump and system curves.

H = Head

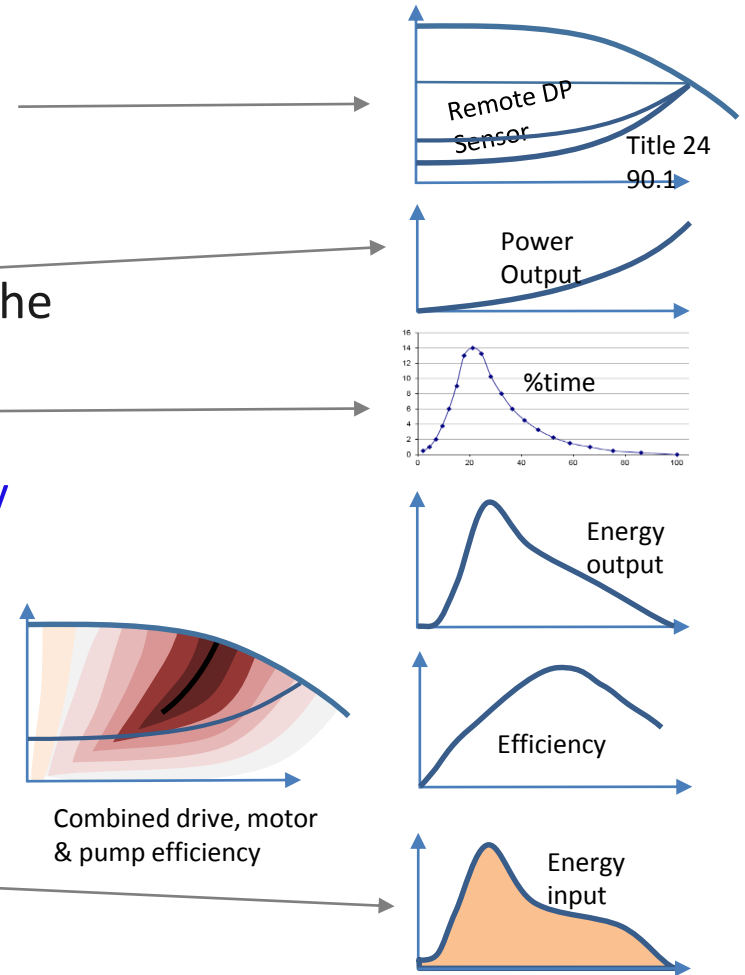
Q = Flow

● = operating point

# Pump Selection Process

# Annual Energy Use Estimation

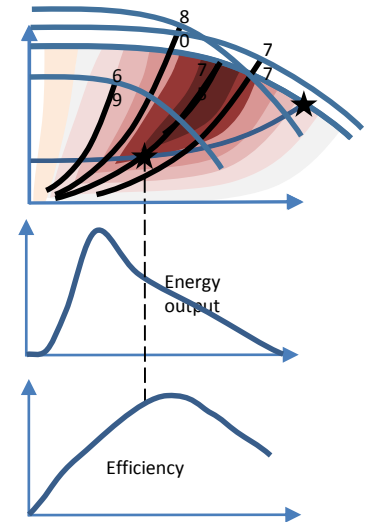
- Step 1 – Determine the **Control Method**
- Step 2 – Calculate the **Power Delivered** at each flow: Flow x Diff Press
- Step 3 – Use the flow profile to determine the pump **Energy Output** profile:  
Pwr x hrs
- Step 4 – Determine the pump/fan **Efficiency** at each flow for the control method
- Step 5 – Calculate the **Energy Input** profile (Energy output / Eff) and integrate



# Best Energy Efficiency Estimation

- If we have to select a pump in a group, the one which will use minimum energy input, maximizes the correlation between Efficiency and Energy output
- This happens for the pump which has its best efficiency curve closest to the Energy output “center of mass”
- The information usually available is the efficiency curves and values
- The pump has to be able to provide the design day flow and diff pressure

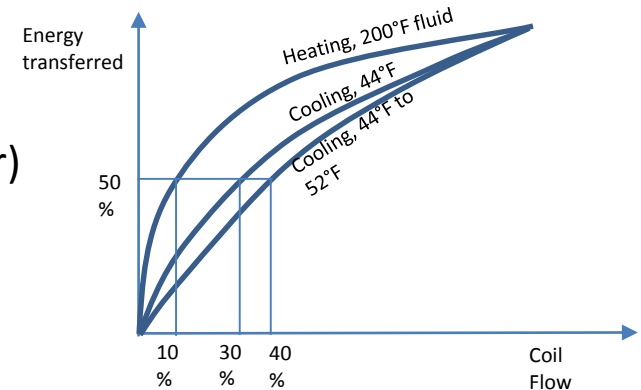
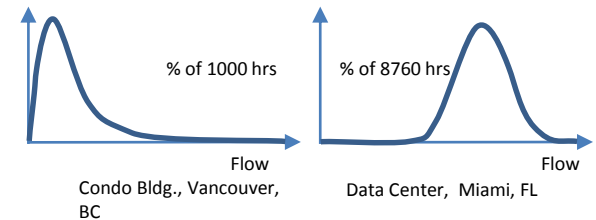
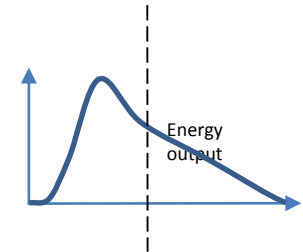
Smart selection of the right equipment for the application





# Best Energy Efficiency Selection

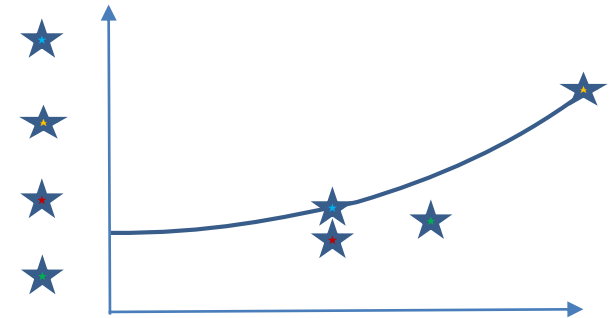
- The determination of the output energy “center of mass” depends heavily on the **flow profile**
- The flow profile depends on:
  1. The **type of building** (school, residential, hospital, data center, mixed...), which determine the occupancy patterns and use. I.e. **internal loads profile**
  2. The **location** (weather) and **building insulation**. I.e. **external load profile**
  3. The presence of **heat recovery** and **free air cooling**
  4. The pump **application** (primary, secondary, condenser)
  5. The fluid **type** and **temperature control** method



# Best Energy Efficiency Selection – Rules of Thumb

If all that info is not available, then use the following “center of mass”, relative to the design day flow and head:

		Flow	Head
• Secondary pumps	0.5	0.65	
• Primary pumps in VP/VS	1	1	
• Distribution primary pumps	0.5	0.4	
• VS condenser pumps	0.7	0.5	



- CS condenser pumps should be designed for 12 to 14°F design day  $\Delta T$   
(see “Optimizing Design & Control of Chilled Water Plants Part 4 Chiller & Cooling Tower Selection”, ASHRAE Journal, Mar 2012)

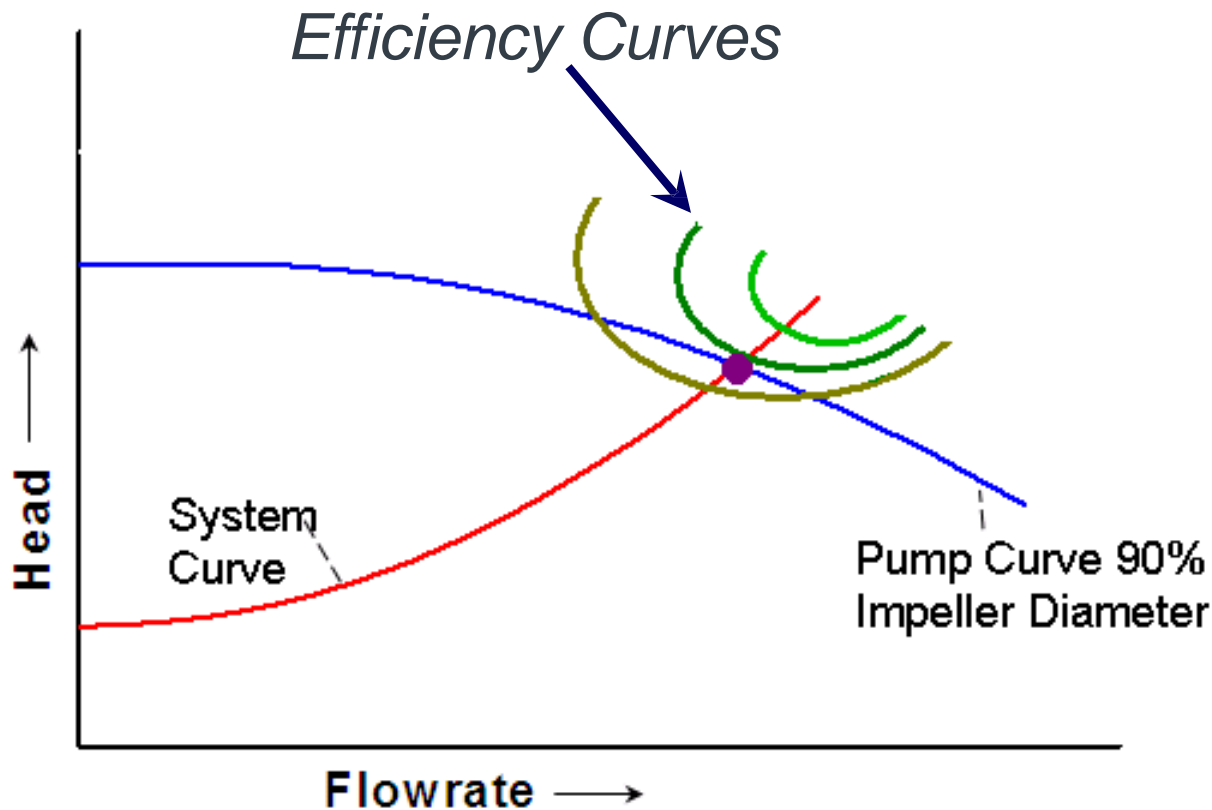
# Life Cycle Costs: Energy Is Only Part Of The Story

	Constant Speed Pump	Variable Speed Pump	Smart Pump
Initial Cost	\$150,000	\$200,000	\$215,000
Installation Cost	\$34,500	\$47,000	\$37,000
Annual KwhR (Reactive)	140,515	58,789	58,789
Total Energy Cost (P.V.)	\$174,961	\$73,200	\$53,200
Operating Cost (P.V.)	\$451,300	\$338,475	\$305,116
Repair/Maint. Cost (P.V.)	\$56,412	\$66,715	\$45,652
Downtime Cost (P.V.)	\$112,825	\$98,615	\$56,000
Environmental Cost (P.V.)	\$5,614	\$5,614	\$5,614
Disposal Cost (P.V.)	\$232	\$232	\$232
Scrap Value (P.V.)	(\$673)	(\$673)	(\$673)
Depreciation (P.V.)	(\$45,168)	(\$52,251)	(\$52,251)
Present Value of Cost	<b>\$940,003</b>	<b>\$776,927</b>	<b>\$664,890</b>

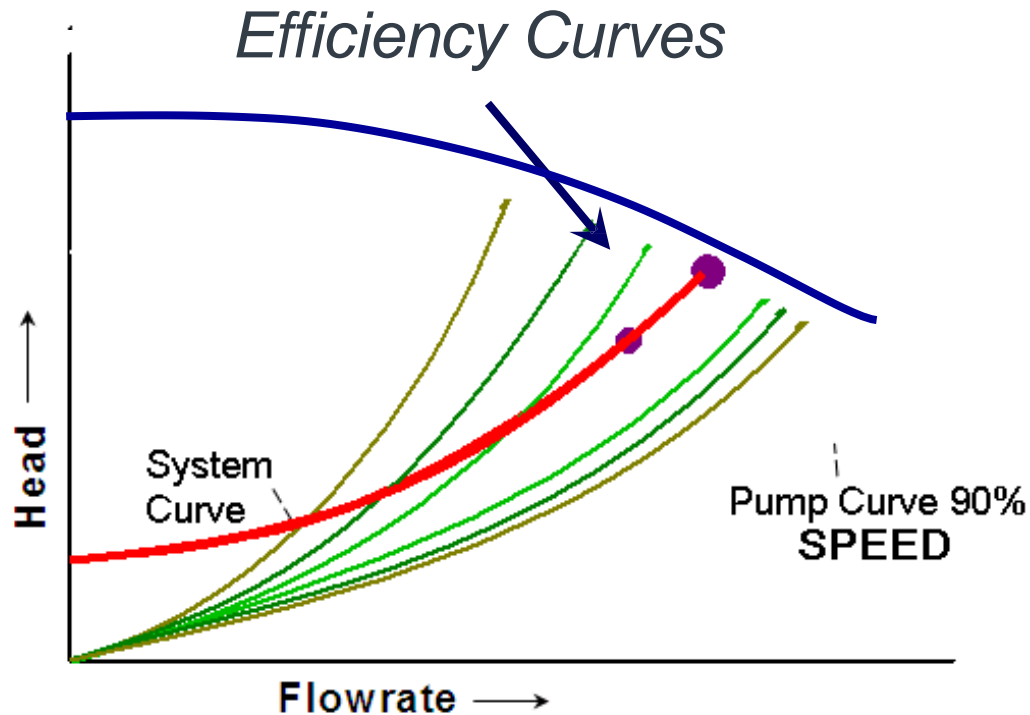
- 20 year life cycle
- Annual Discount Rate 6%
- Customer Tax Rate 31%
- Straight Line Depreciation Over 7 Years
- \$0.1 per kWh
- Energy cost increases 5%/year
- Non-energy inflation 4%

The above is an example to give relative cost information

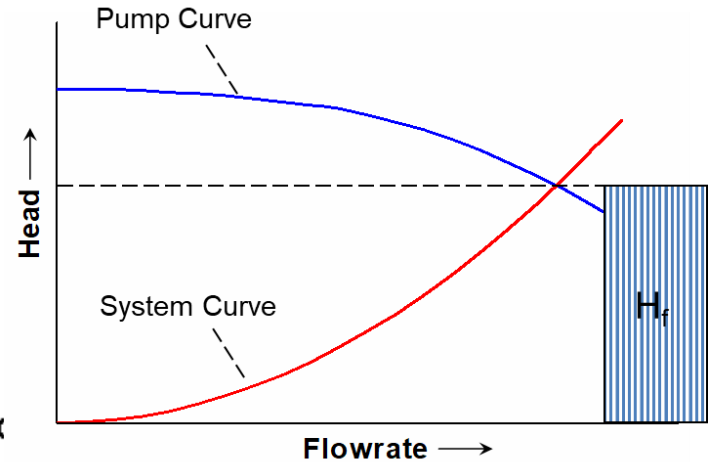
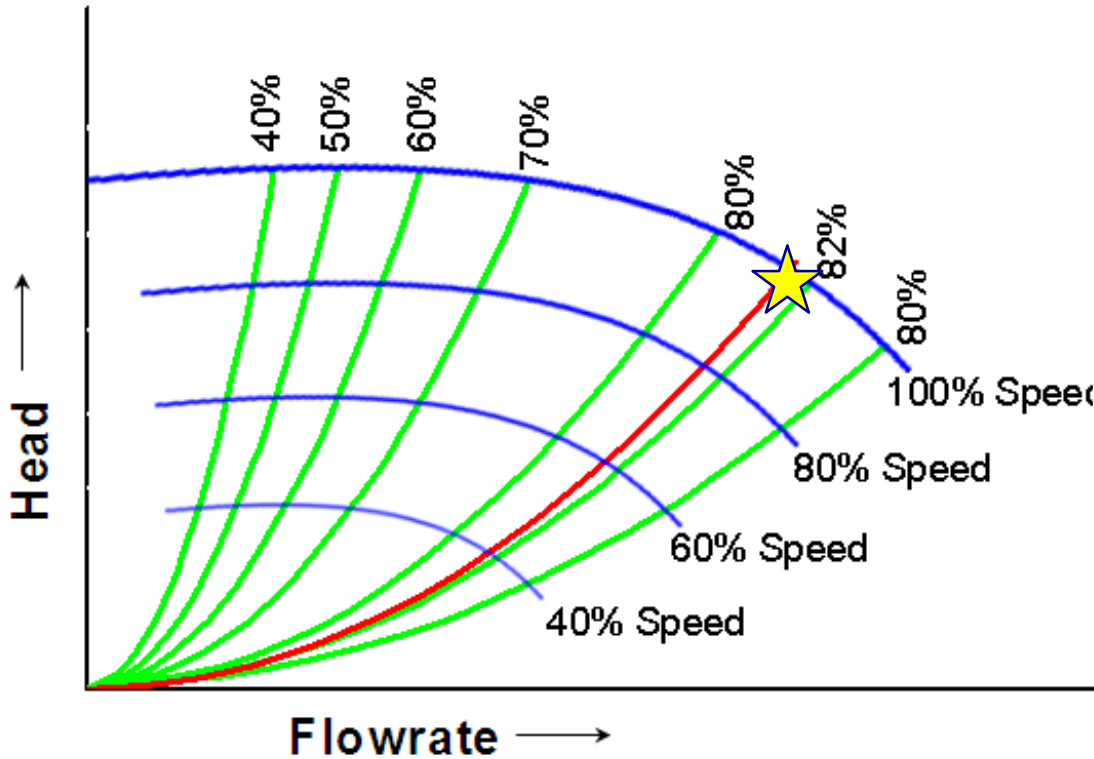
# Adjusting for Impeller Diameter



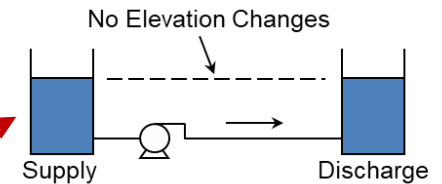
# Adjusting Pump Head Curve for Different Speeds



# Friction-Dominated System

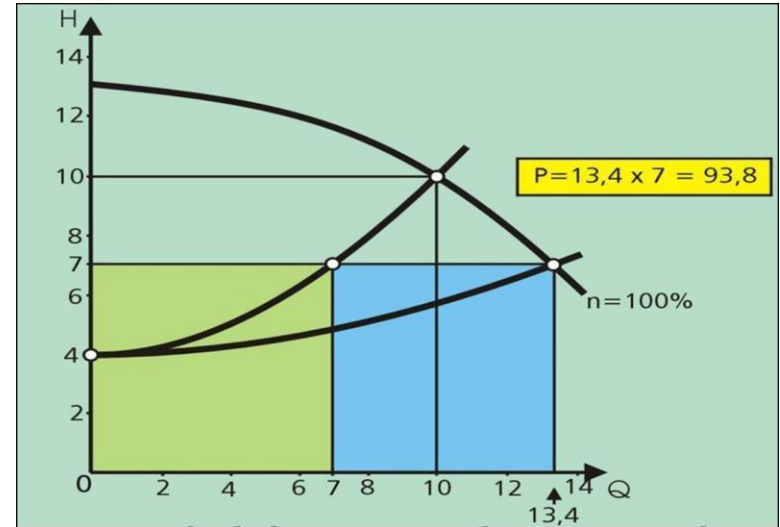
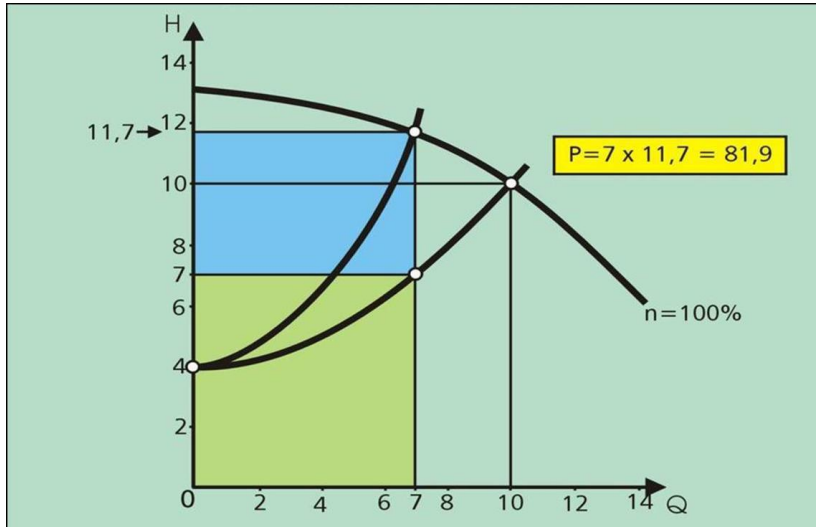


Example:



Any pump can produce flow (no elevation to overcome)

# Indicators of Poor System Energy Optimization



- Valve throttling increases system head resulting in excess power consumption
- Excess energy noted in blue area
- Excess energy impacts equipment reliability

- Bypass lines require more flow, which results in excess power consumption.
- Excess energy impacts equipment reliability





# Suction Specific Speed NSS Calculator

## Suction Specific Speed (NSS) Calculator

<b>N =</b>	<b>3560</b>	<b>Pump Shaft Rotation Speed (rpm)</b>
<b>Q =</b>	<b>800</b>	<b>Flow Rate Capacity (m<sup>3</sup>/h, m<sup>3</sup>/min, US gpm, British gpm) at Best Efficiency Point (BEP)</b>
<b>NPSHr =</b>	<b>18</b>	<b>Required Net Positive Suction Head for the pump at the BEP (m, ft)</b>
<b>NSS =</b>	<b>8147.5</b>	<b>Suction Specific Speed</b>

**Rule of Thumb:**

**Nss Should be Below 8500 with US GPM, to Avoid Cavitation**

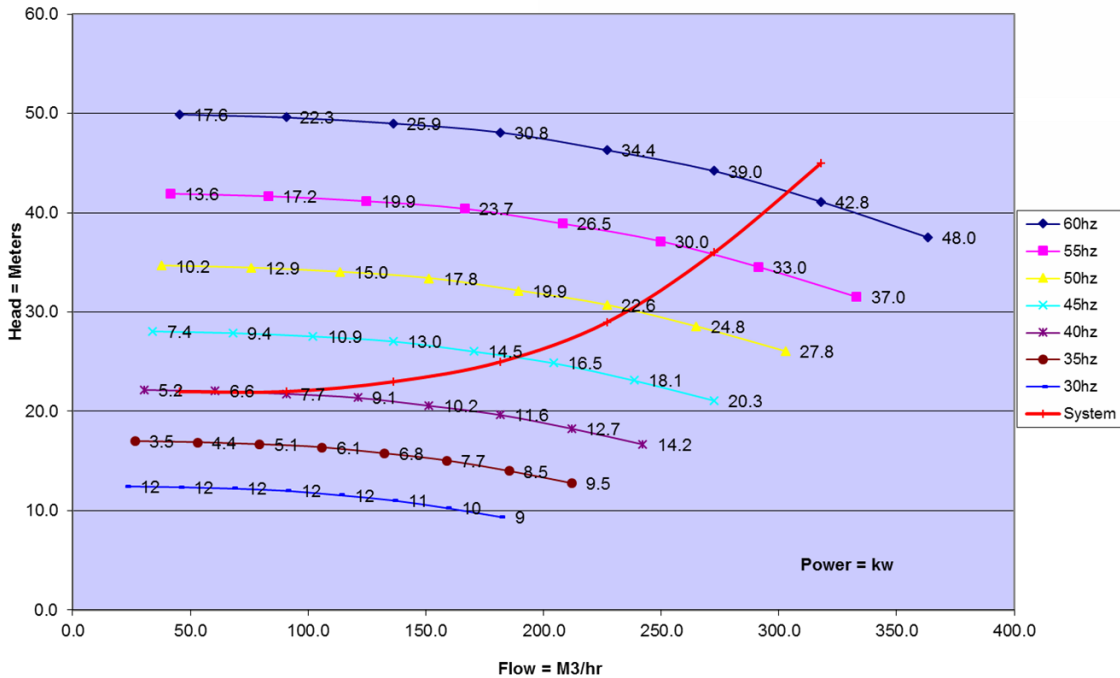
# Variable Speed Pumping Analyzer

1	Aurora 5X6X12 12" Trim 1750RPM
2	Flow = M3/hr
3	Head = Meters
4	Power = kw

Q1	Q2	Q3	Q4	Q5	Q6	Q7	Q8	H1	H2	H3	H4	H5	H6	H7	H8
45.4	90.8	136.2	181.7	227.1	272.5	317.9	363.3	49.9	49.6	49.0	48.1	46.3	44.2	41.1	37.5

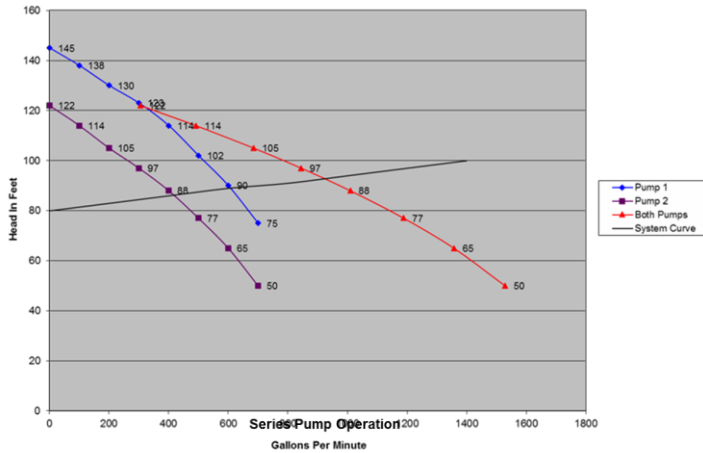
SH1	SH2	SH3	SH4	SH5	SH6	SH7	SH8
22.0	22.0	23.0	25.0	29.0	36.0	45.0	

P 1	P 2	P 3	P 4	P 5	P 6	P 7	P 8
17.6	22.3	25.9	30.8	34.4	39.0	42.8	48.0

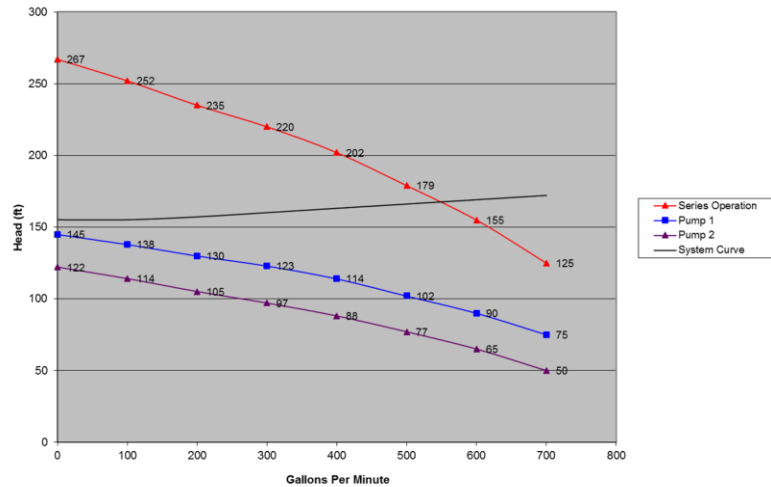


# Series/Parallel Calculator

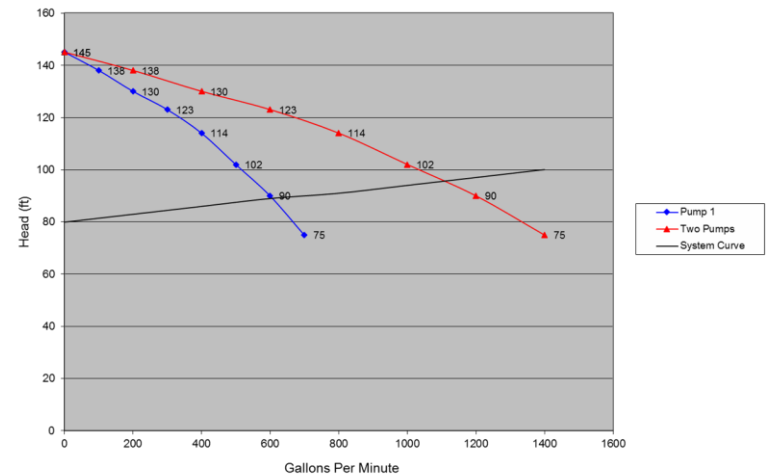
Parallel Operation Similar Pumps (Pumps 1 & 2)



FLOW / HEAD	Q1 / H1	Q2 / H2	Q3 / H3	Q4 / H4	Q5 / H5	Q6 / H6	Q7 / H7	Q8 / H8
FLOW	0	100	200	300	400	500	600	700
HEAD PUMP 1	145	138	130	123	114	102	90	75
HEAD PUMP 2	122	114	105	97	88	77	65	50
SYS CURVE (SER)	155	155	157	160	163	166	169	172
SYS CURVE (PAR)	80	83	86	89	91	94	97	100



Parallel Operation Identical Pumps (Pump 1)



# Darcy Friction Loss Calculator

<b>Given Data</b>						
Flow Rate (Q)	m3/hr	8	0.00222	m3/s		INPUTS
Pipe Inside Diameter (D)	mm	53.7	0.0537	m		CALCULATED VALUES
Kinematic Viscosity ( $\nu$ )	cSt	1	1.000E-06	m2/s		
Specific Roughness ( $\epsilon$ )	m	1.50E-06				
Pipe Length (L)	m	230				
<b>Calculated Data</b>						
Average Velocity - V (m/s)		0.98				
Reynolds Number		52689				
Darcy Friction Factor		0.021				
<b>Head Loss - Pipe (m)</b>		<b>4.34</b>				
					<b>TOTAL HEAD LOSS, <math>h_f</math> (m)</b>	<b>5.06</b>
<b>Calculated Head Loss in Fittings, Valves, Entrances &amp; Exits</b>						
		<b>K</b>	<b>Qty</b>	<b>Sub Total K</b>		
Angle Valve		5	0	0		
Ball Valve, Full Port		0.05	2	0.1		
Butterfly Valve		0.6	0	0		
Check Valve, Swing Type		2.3	1	2.3		
Elbow 45 Degrees		0.4	0	0		
Elbow 90 Degrees, Long Radius		0.6	0	0		
Elbow 90 Degrees, Standard		0.9	12	10.8		
Flow Meter, Turbine Type		7	0	0		
Foot Valve		0.9	0	0		
Gate Valve		0.2	0	0		
Globe Valve		10	0	0		
Pipe Entrance, Inward Projected Pipe		1	0	0		
Pipe Entrance, Sharp Edge		0.5	1	0.5		
Pipe Exit		1	1	1		
Tee, Standard, Flow Through Branch		1.8	0	0		
Tee, Standard, Flow Through Run		0.6	0	0		
				<b>14.7</b>		
<b>Head Loss - Valves &amp; Fittings (m)</b>		<b>0.72</b>				

# System Energy Calculator

Required Data	Option 1	Option 2
System Condition:	Steel Pipe	Steel Pipe
	8" 600'	6" 600'
Pump Operation - Hours / Day	8	8
Pump Operation - Days / Year	365	365
Pump Flow - GPM	600	600
Pump Head - Feet	50	65
Pump Efficiency - %	71%	71%
Motor Efficiency - %	82.0%	82.0%
Energy Cost in \$/KWH	\$0.11	\$0.11
<b>Results</b>		
BHP At Design Point	10.7	13.9
Wire to Water Efficiency - %	58%	58%
Annual Energy Cost	\$3,117.94	\$4,053.33
KW Per 1000 Gallons Pumped	0.270	0.351
Cost Per 1000 Gallons Pumped	\$0.030	\$0.039
<b>PAYBACK</b>		
Annual Savings - \$\$	\$935.38	
Annual Savings - %	23.08%	
Cost of Option 1	\$12,000.00	
Cost of Option 2	\$9,000.00	
Payback - Years	3.2	

# Motor Yearly Energy Cost Calculator

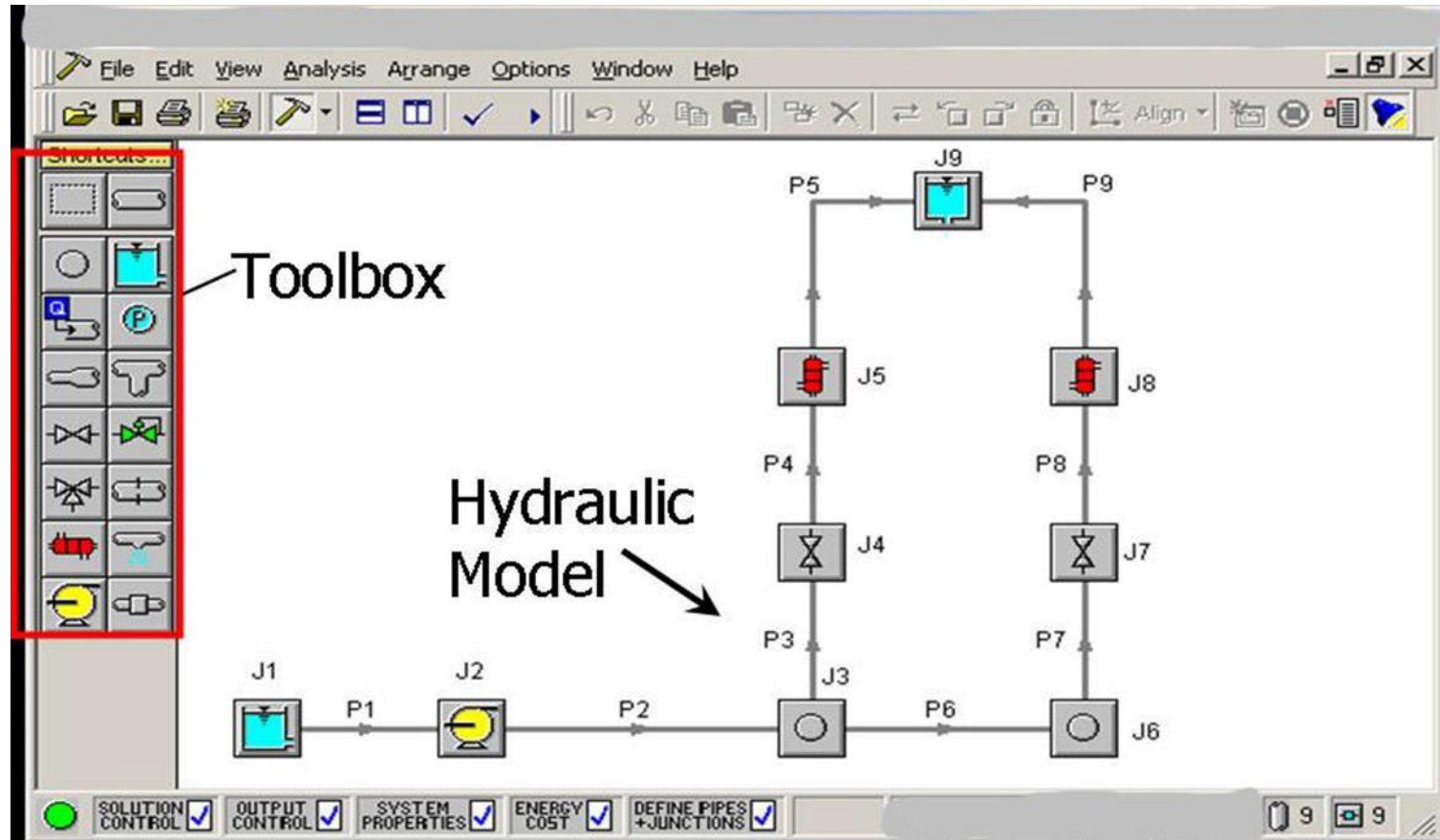
Site Energy Cost (KW/Hour)		Site Demand Charge (KVA/Year)		Estimated Motor Usage (Hrs/Year)	
	\$0.060		\$75.00		8760
<b>Synchronous Motor Characteristics</b>			<b>Induction Motor Characteristics</b>		
Horsepower		Horsepower			
Power Factor		Power Factor			
Efficiency		Efficiency			
Kilowatts		Kilowatts			
Total KVA		Total KVA			
Yearly Energy Cost		Yearly Energy Cost			
Yearly Demand Cost		Yearly Demand Cost			
<b>Synchronous Yearly Energy Savings Due to Efficiency</b>					
<b>Synchronous Yearly Energy Savings Due to Demand</b>					
<b>Total Yearly Energy Savings Using Synchronous Motor Technology</b>					
<b>Total Life Cycle Energy Savings Using Synchronous Motor Technology (per motor)</b>					

# PSIM Tool



**PUMP  
SYSTEM  
IMPROVEMENT  
MODELING TOOL**

# Case Study Using PSIM





# Building the Model Using PSIM

**Pump Configuration**

Flow Parameter:  Volumetric (gal/min)  Mass

Pressure/Head Parameter:  Head (feet)  Pressure

Efficiency/Power:  Efficiency (Percent)  Power

Pump Data | Configuration Data | Composite Graph | Pump Graph | NPSHR Graph | Efficiency Graph

Raw Data:  Optional Data

Data Point	Q (gal/min)	dH (feet)	NPSHR (feet)	Efficiency (Percent)
1	0	270	5	0
2	50	270	5	35
3	100	270	6	60
4	150	270	8	74
5	200	267	11	82
6	250	250	16	85
7	300	220	21	80
8	350	180	25	65
9	400	150	30	55
10				
11				
12				
13				
14				
15				

Curve Fitting: Curve Fit Type: **Polynomial** (Interpolated X-Y Data) Curve Fit Order: 2

Head Rise  All  None  Invert

Net Positive Suction Head Required

Efficiency

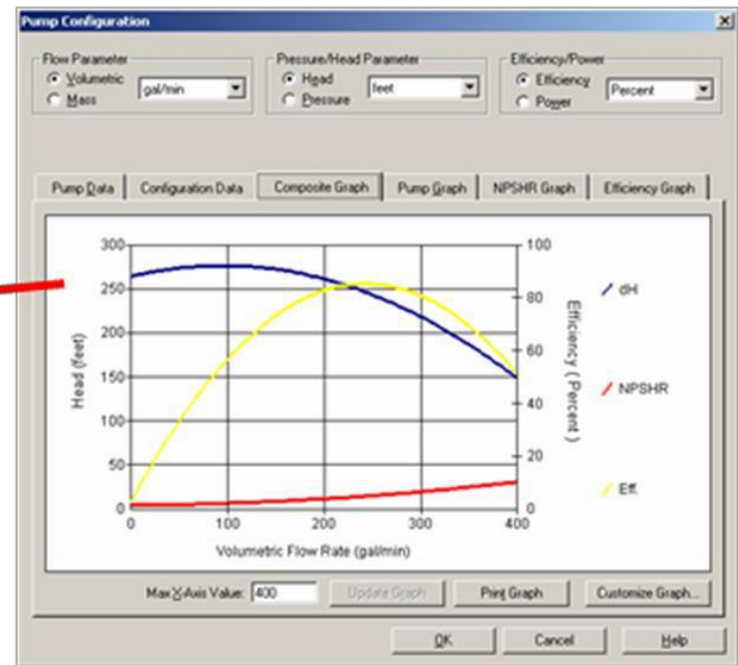
Generate Curve Fit Now

$$\Delta H = a + bQ + cQ^2 + dQ^3 + eQ^4$$

PUMP CURVE	
a	264.3333
b	0.262381
c	-1.380952E-03
NPSH	
a	4.406061
b	6.08658E-03
c	1.497835E-04
EFFICIENCY	

Edit Table

OK Cancel Help



# Entering the Pipe Data

**Pipe Specifications**

Number: 1      Upstream Junction: 1  
Name: Pipe      Downstream Junction: 2  
Copy Data From Pipe...      Copy Previous...

OK  
Cancel  
Help

Pipe Model | **Fittings & Losses** | Optional | Status

Size

Pipe Material: Steel  
Pipe Geometry: Cylindrical Pipe  
Size: 4 inch  
Type: STD (schedule 40)  
Inner Diameter: 4.026 inches

Length: 20 feet  
feet  
inches  
microinches  
miles

Friction Model

Data Set: Unspecified  
Standard

Absolute Roughness: 0.0018 inches  
Load Default

# System Predictions Based on Model

File Edit View Analysis Arrange Options Window Help

Show: General, Pipes and Junctions

General Warnings Cost Report **Pump Summary** Valve Summary Heat Exchanger Summary Reservoir Summary

Jct	Name	Vol. Flow (gal/min)	dH (feet)	Overall Efficiency (Percent)	Overall Power (hp)	Energy Cost (U.S. Dollars)	BEP (gal/min)	% of BEP (Percent)	NPSHA (feet)	NPSHR (feet)
2	Pump	367.4	174.3	63.85	25.36	63,261	243.0	151.2	60.13	26.86

Pipes

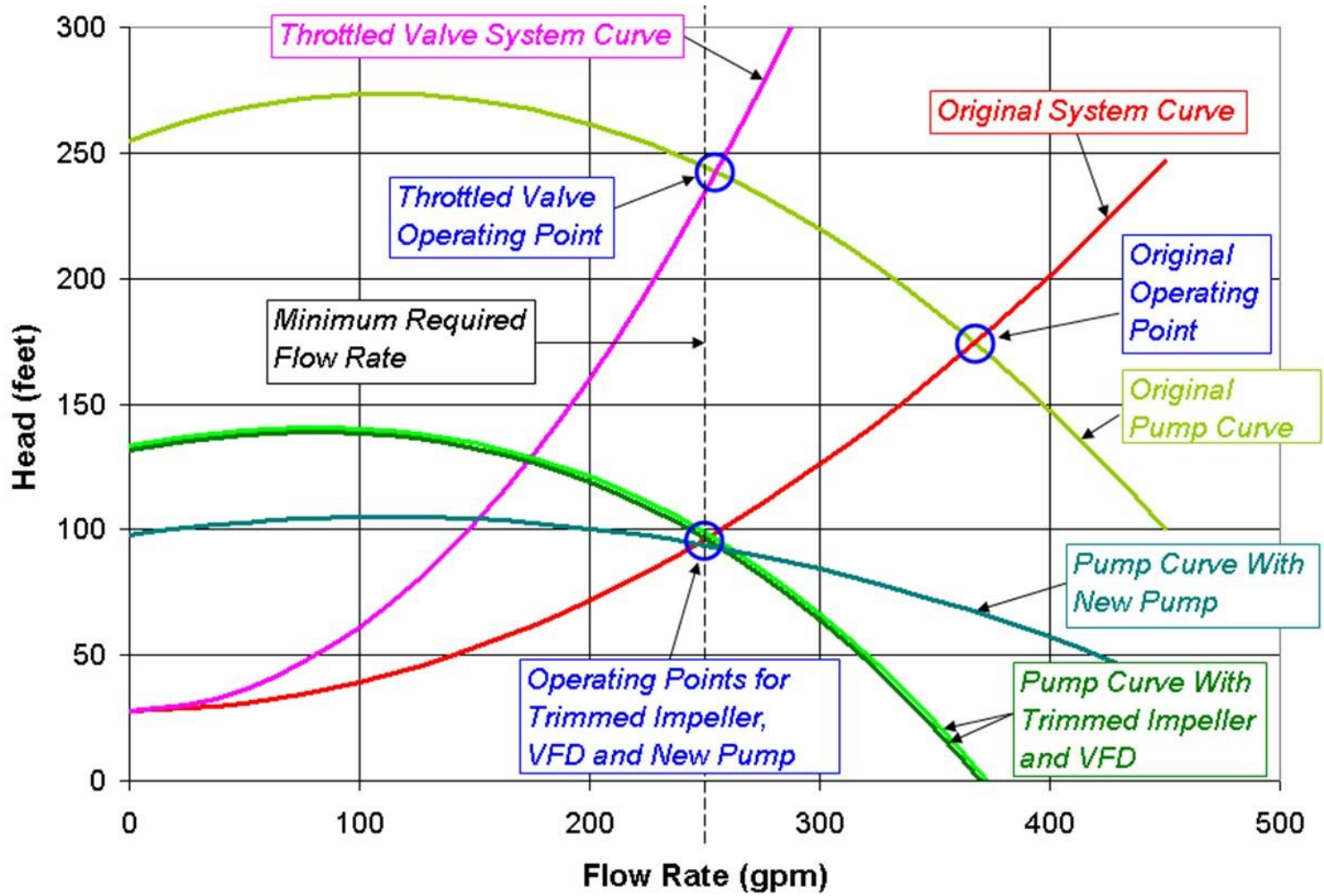
Pipe	Name	Vol. Flow Rate (gal/min)	Velocity (feet/sec)	P Static Max (psia)	P Static Min (psia)	dP Stag. Total (psid)	dP Static Total (psid)	dH (feet)	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)
1	Pipe	367.4	9.260	26.29	25.65	0.6328	0.6328	1.460	26.29	25.65	26.86	26.23
2	Pipe	367.4	9.260	101.20	99.62	1.5818	1.5818	3.649	101.20	99.62	101.78	100.20
3	Pipe	184.3	7.997	99.77	97.76	2.0053	2.0053	4.627	99.77	97.76	100.20	98.19

All Junctions Database Sources Branch Heat Exchanger Pump Reservoir Valve

Jct	Name	P Static In (psia)	P Static Out (psia)	P Stag. In (psia)	P Stag. Out (psia)	Vol. Flow Rate Jct Net (gal/min)	Mass Flow Rate Jct Net (lbm/sec)	Loss Factor (K)
1	Supply Tank	24.70	26.86	24.70	26.86	-367.4	-51.09	0.00
2	Pump	25.65	101.20	26.23	101.78	0.0	0.00	0.00
3	Tea/Water	99.77	99.77	100.20	100.20	0.0	0.00	0.00

SOLUTION CONTROL  OUTPUT CONTROL  SYSTEM PROPERTIES  ENERGY COST  DEFINE PIPES + JUNCTIONS

# Graphically-Illustrated Options



# Hot Water World



## APPLICATION OVERVIEW



RESOURCE: [http://www.grundfos.com/content/dam/Global%20Site/campaigns/Grundfos-isolutions/5/download-pdfs/1013669\\_GFS\\_CBS\\_Poster\\_A0\\_841x1189\\_ART10\\_CM.pdf](http://www.grundfos.com/content/dam/Global%20Site/campaigns/Grundfos-isolutions/5/download-pdfs/1013669_GFS_CBS_Poster_A0_841x1189_ART10_CM.pdf)

# Piping and Pumping Systems Can Be Very Complex



# Pump System Types in Commercial Buildings

## 1. Temperature Control

- a) Heating system applications
- b) Cooling system applications

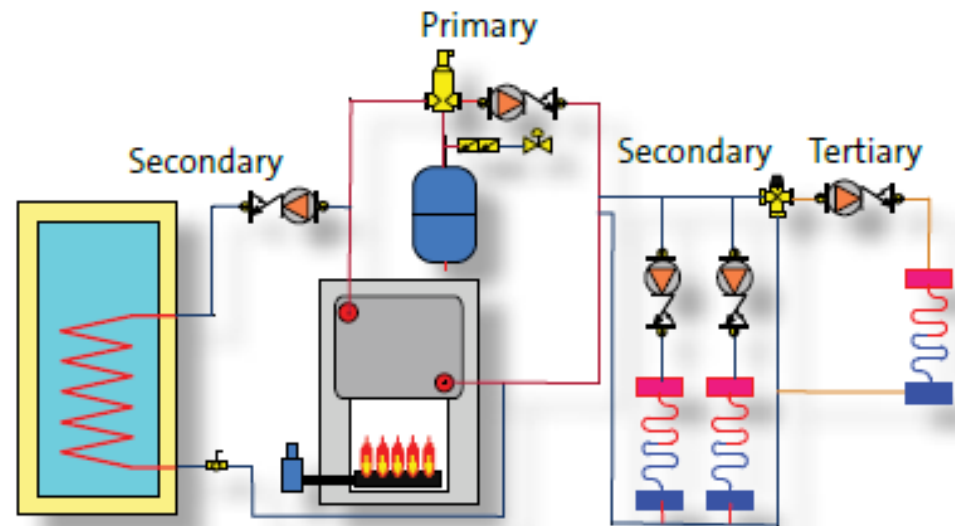
## 2. Plumbing systems

- a) Domestic water applications
- b) Drainage applications



# Heating Applications

- Primary, secondary and tertiary loops
- Mixing loops
- Steam
  - Boiler feed
  - Condensate return
  - Etc.
- Geothermal
- Solar
- District heating

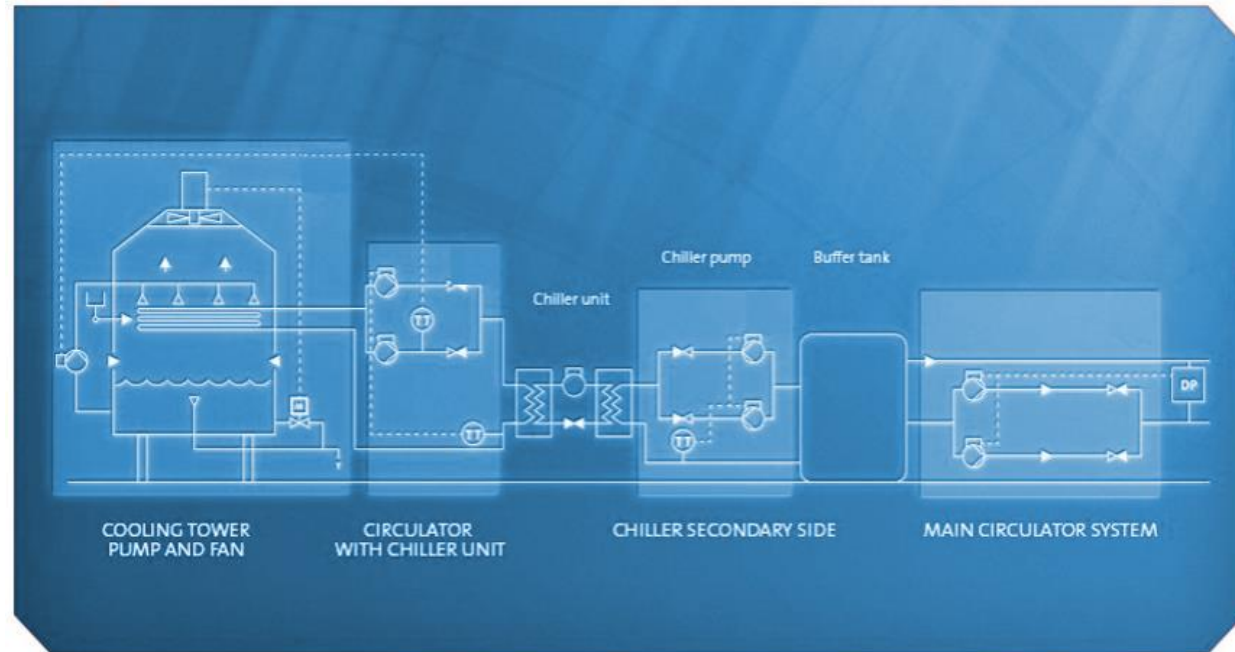


# Heating Optimization Targets

Primary, Secondary, and Tertiary loops	X
Mixing loops	
Steam:	
Boiler Feed	X
Condensate return	
Collection tank pumps	
Water treatment pumps	
Deaerator tank recycle pumps	
Economizer pumps	X
Deaerator vacuum pumps (vacuum deaerator tanks only)	
Geothermal	
Solar	
District heating	X

# Cooling Applications

- Primary, Secondary, and Tertiary loops
- Condenser water
- Thermal energy storage
- Cooler tower
- Geothermal
- District cooling



# Cooling Optimization Targets

Primary, Secondary, and Tertiary loops	X
Condenser water	X
Cooling tower	X
Thermal energy storage	
Geothermal	
District cooling	X

# Domestic Water Applications

- Booster system
  - With break tank
  - With connection to water main
  - With roof tank
- Water transfer to roof tank
- Hot water recirculation
- Landscaping
- Swimming pool



# Domestic Water Optimization Targets

Booster system:	
With Hydro-pneumatic tank	X
With connection to water main	X
With roof tank	
Water transfer to roof tank	
Hot water recirculation	X
Landscaping	X
Swimming pool	

# Drainage Applications

- Storm drainage
- Drainage from facility rooms
- Emptying of pools and tanks
- Laundry
- Effluent/sewage
- Elevator sump
- Parking garages



# Drainage Optimization Targets

Storm drainage	X
Parking garages	X
Drainage from facility rooms	
Laundry	
Emptying of pools and tanks	
Effluent/sewage	X
Elevator sump	



# Example: Domestic Water Pressure Booster Optimization



# Domestic Pressure Boosting Example – Specification (Open System)

Constant pressure system – 50 psi

Multi-story building

Duty point – 400 gpm at 300 feet

Second flow point – 300 gpm

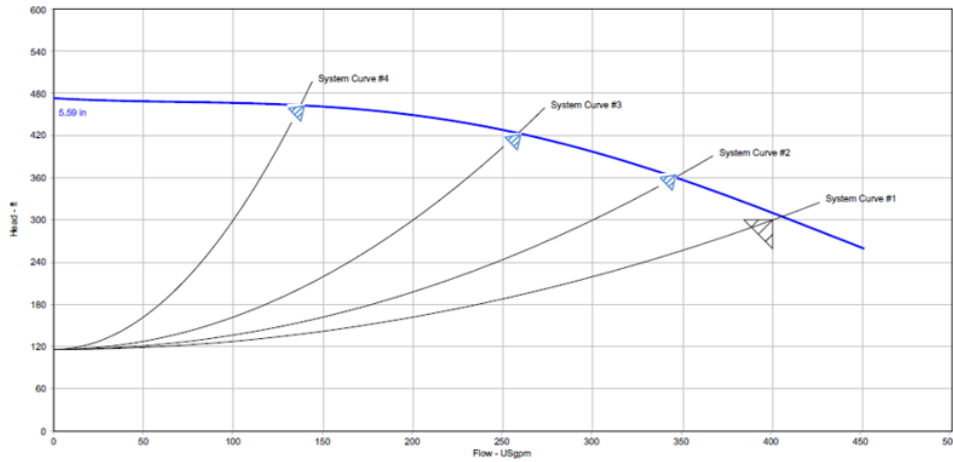
Third flow point – 200 gpm

Fourth flow point – 100 gpm

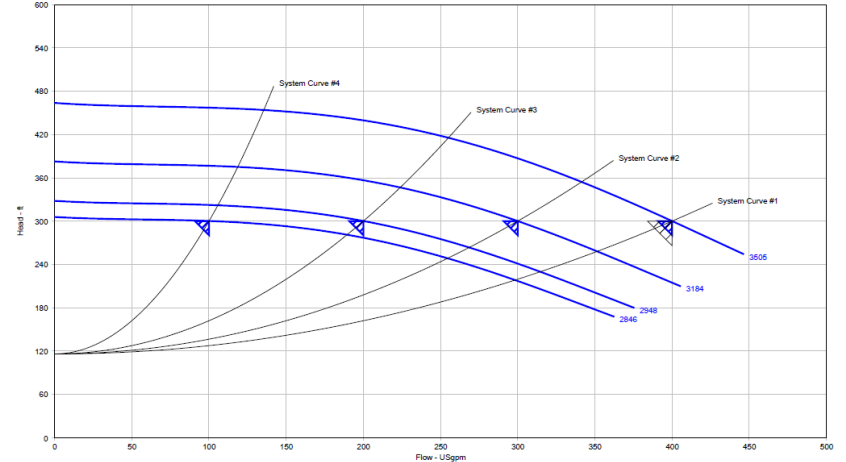
Load profile – next slides

50 psi municipal water supply

# Curve Comparison



**Fixed Speed Pump**



**Variable Speed Pump**

# Annual Power Consumption

## Fixed Speed Pump

Expected pump life: 1 years	Load Profile #1	Load Profile #2	Load Profile #3	Load Profile #4	Load Profile #5	Total
Flow: ( USgpm )	400.0	300.0	200.0	100.0	-	-
Operation: ( hours per year )	250	500	1,000	2,000	-	3,750
Energy cost, present value ( per kWh)	0.1000	0.1000	0.1000	0.1000	-	-
Speed, rated (rpm)	3540	3540	3540	3540	-	-
Head (ft)	310.0	396.9	449.1	466.4	-	-
Efficiency (%)	75.03	77.97	68.33	43.97	-	-
Rated power (based on duty point) (hp)	41.73	38.56	33.18	26.78	-	-
Motor efficiency (%)	93.00	94.00	93.00	92.00	-	-
Drive/gear efficiency (%)	100.00	100.00	100.00	100.00	-	-
System curve	System Curve #1	System Curve #2	System Curve #3	System Curve #4	-	-
Energy, total (kWh)	8,364.2	15,292.9	26,607.6	43,410.6	-	93,675.5
Energy cost, per year	836.42	1,529.29	2,660.76	4,341.06	-	9,367.55
Energy cost, total present value	812.75	1,486.01	2,585.46	4,218.20	-	9,102.43

## Variable Speed Pump

Expected pump life: 1 years	Load Profile #1	Load Profile #2	Load Profile #3	Load Profile #4	Load Profile #5	Total
Flow: ( USgpm )	400.0	300.0	200.0	100.0	-	-
Operation: ( hours per year )	250	500	1,000	2,000	-	3,750
Energy cost, present value ( per kWh)	0.1000	0.1000	0.1000	0.1000	-	-
Speed, rated (rpm)	3505	3184	2948	2846	-	-
Head (ft)	300.0	300.0	300.0	300.0	-	-
Efficiency (%)	74.65	78.36	73.79	51.48	-	-
Rated power (based on duty point) (hp)	40.59	29.00	20.54	14.72	-	-
Motor efficiency (%)	93.00	92.00	83.00	70.00	-	-
Drive/gear efficiency (%)	97.00	96.00	95.00	91.00	-	-
System curve	System Curve #1	System Curve #2	System Curve #3	System Curve #4	-	-
Energy, total (kWh)	8,388.3	12,244.3	19,425.8	34,466.7	-	74,525.1
Energy cost, per year	838.83	1,224.43	1,942.58	3,446.67	-	7,452.51
Energy cost, total present value	815.09	1,189.77	1,887.60	3,349.13	-	7,241.59

# Annual power consumption

Fixed Speed Pump

Expected pump life: 1 years	Load Profile #1	Load Profile #2	Load Profile #3	Load Profile #4	Load Profile #5	Total
Flow: ( USgpm )	400.0	300.0	200.0	100.0	-	-
Operation: ( hours per year )	250	500	1,000	2,000	-	3,750
Energy cost, present value ( per kWh)	0.1000	0.1000	0.1000	0.1000	-	-
Speed, rated (rpm)	3540	3540	3540	3540	-	-
Head (ft)	310.0	300.0	449.1	466.4	-	-
Efficiency (%)	75.0	77.9	68.7	43.0	-	-
Rated power (based on duty point) (hp)	41.75	38.56	33.18	26.78	-	-
Motor efficiency (%)	93.00	94.00	93.00	92.00	-	-
Drive/gear efficiency (%)	100.00	100.00	100.00	100.00	-	-
System curve	System Curve #1	System Curve #2	System Curve #3	System Curve #4	-	-
Energy, total (kWh)	8,364.2	15,292.9	26,607.6	43,410.6	-	93,675.3
Energy cost, per year	836.42	1,529.29	2,660.76	4,341.06	-	9,367.55
Energy cost, total present value	812.75	1,486.01	2,585.46	4,218.20	-	9,102.43

Variable Speed Pump

Expected pump life: 1 years	Load Profile #1	Load Profile #2	Load Profile #3	Load Profile #4	Load Profile #5	Total
Flow: ( USgpm )	400.0	300.0	200.0	100.0	-	-
Operation: ( hours per year )	250	500	1,000	2,000	-	3,750
Energy cost, present value ( per kWh)	0.1000	0.1000	0.1000	0.1000	-	-
Speed, rated (rpm)	3505	2985	2948	2846	-	-
Head (ft)	300.0	300.0	300.0	300.0	-	-
Efficiency (%)	74.6	78.0	73.0	51.0	-	-
Rated power (based on duty point) (hp)	40.00	29.00	20.54	14.72	-	-
Motor efficiency (%)	93.00	92.00	83.00	70.00	-	-
Drive/gear efficiency (%)	97.00	96.00	95.00	91.00	-	-
System curve	System Curve #1	System Curve #2	System Curve #3	System Curve #4	-	-
Energy, total (kWh)	8,388.3	12,244.3	19,425.8	34,466.7	-	74,525.1
Energy cost, per year	838.83	1,224.43	1,942.58	3,446.67	-	7,452.51
Energy cost, total present value	815.09	1,189.77	1,887.60	3,349.13	-	7,241.59

# Advantages of Variable Speed Pumps in Pressure Booster Applications

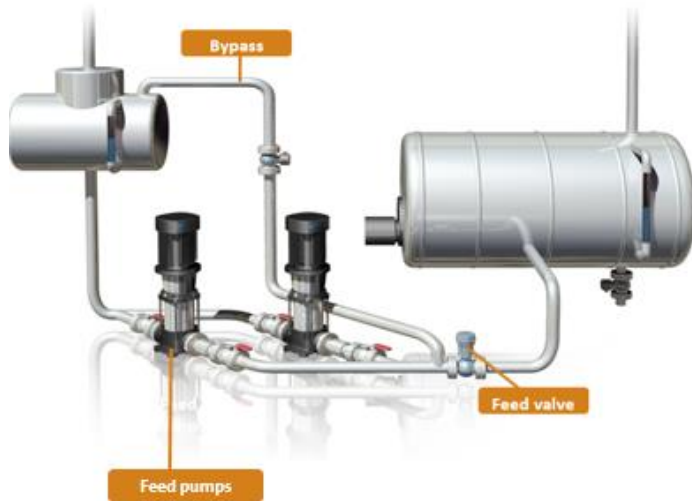
- **Saves at least 30% energy usage**
- Eliminates need for throttling Valves & their energy Loss
- Reduces size of Hydro-pneumatic tank
- Steadier pressures as usage varies – Improved control
- Matches actual flow rate to system requirements
- Reduced wear on pumps/motors- No across line start
- Elimination of water hammer

# Example: Boiler Feed Pump Optimization

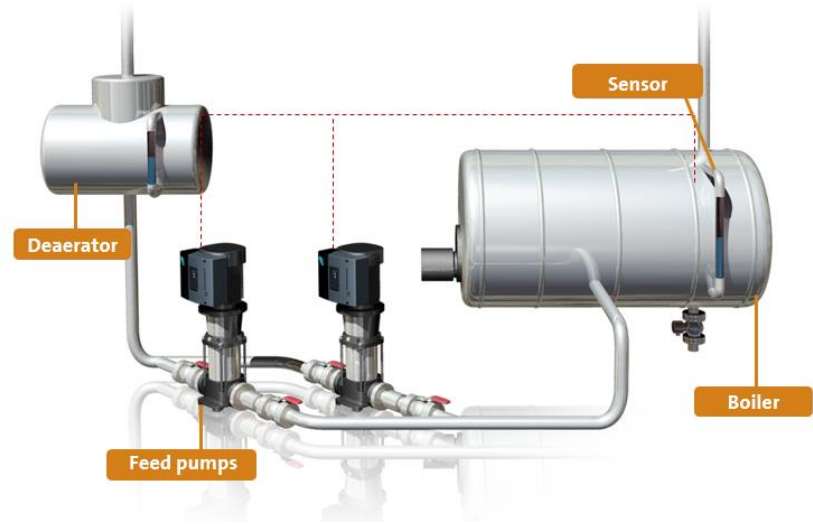


<http://www.bls.gov/ooh/production/stationary-engineers-and-boiler-operators.htm#tab-4>

# Fixed speed pump with feed valve and with bypass line

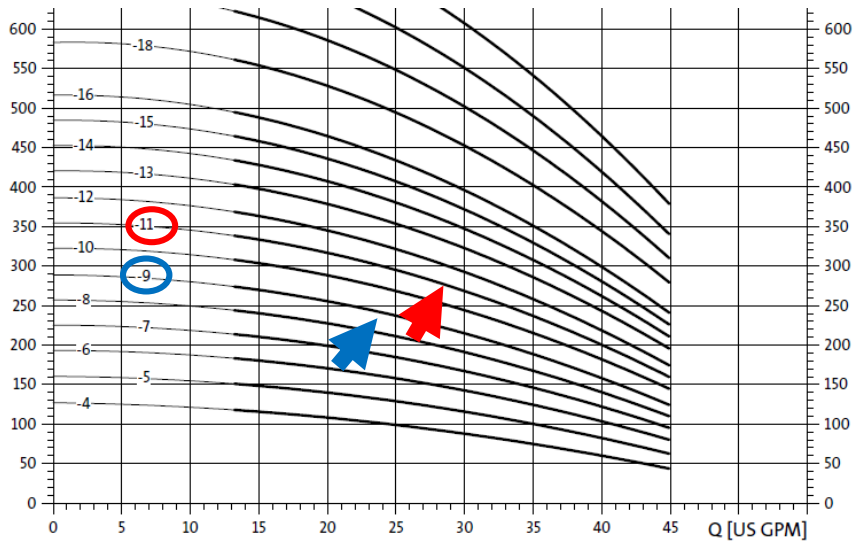


# Variable speed pumps less feed valve and less bypass line

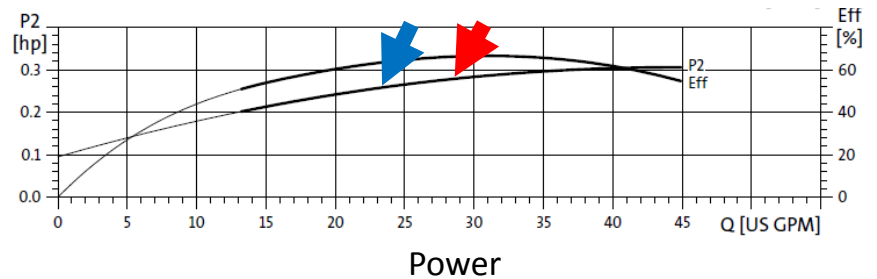




# Fixed Speed Pump vs Variable Speed Pump



Performance Curve



# Summary of Duty Point Performance Characteristics

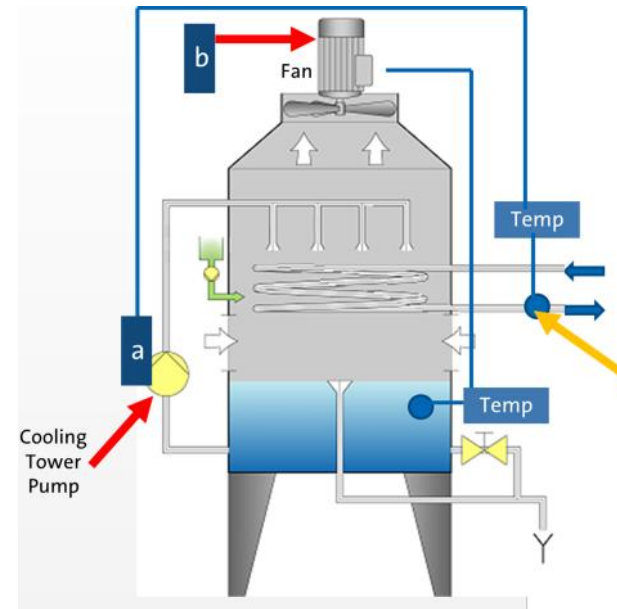
Pump #	Speed Type	Boiler Maximum Horsepower	Use Feed Valve?	Use Bypass Line?	Flow in gpm	Head in feet	Pump Size Inches	Number of Stages	BHP at Duty Point
1	Fixed	250	Yes	Yes	28	272	1.25 x1.25	11	3.0
2	Variable	250	No	No	23	237	1.25 x1.25	9	2.3

*This data shows the potential for power savings at one duty point. But what about at reduced rates of steam production and reduced flow rates? The percentage of savings can be even greater than shown here. And the savings demonstrated in this example can be extended to larger boiler feed systems.*

# Advantages of Variable Speed Pumps in Boiler Feed Applications

- Even steam production
  - Faster reaction with changed speed
  - Smaller loss of water
  - Fewer stages – lower initial cost
  - Eliminate feed valve expense, maintenance, and head loss
  - Eliminate bypass line expense and wasted flow recirculation
  - Smaller HP motor
  - Reduced water treatment costs
  - ***Reduced energy consumption and costs***
- The downside to this variable speed system is that it requires precise commissioning and start-up, and requires highly qualified technicians.

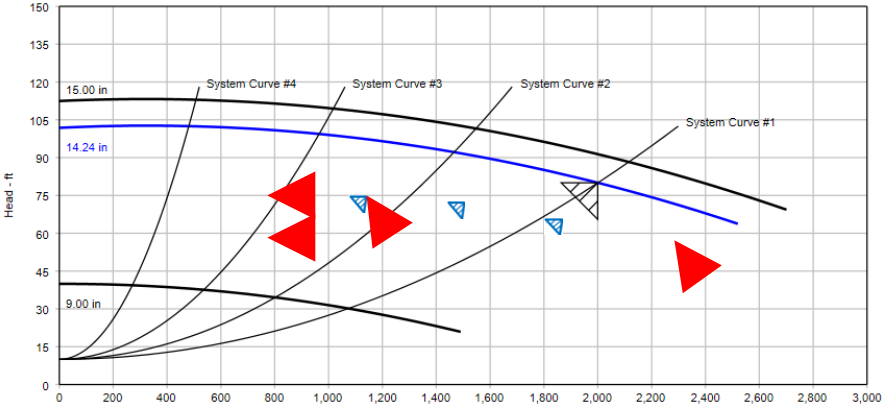
# Example: Cooling Tower Pump Optimization



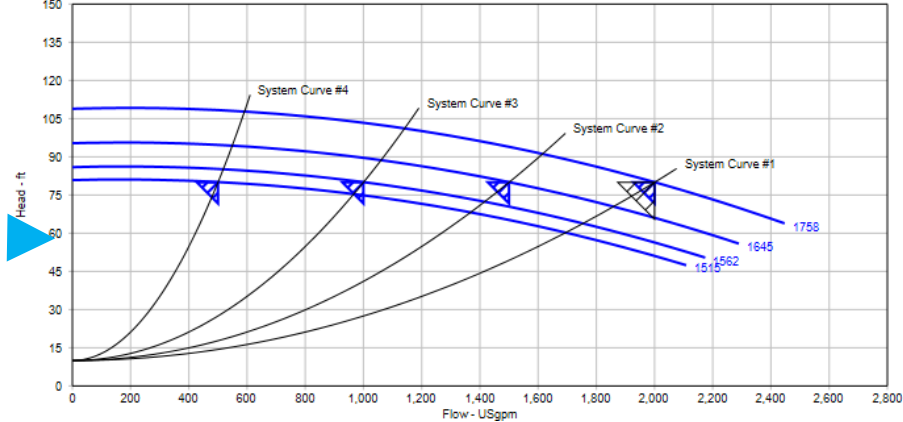
# Cooling Tower Example - Specification

- Duty point = 2000 gpm at 80 feet of head
- Second flow rate point = 1500 gpm
- Third flow rate point = 1000 gpm
- Fourth flow rate point = 500 gpm
- Pump type – Horizontal split case

# Curve Comparison



**Fixed Speed Pump**



**Variable Speed Pump**

$(\text{gpm} \times \text{Feet of Head}) \div \text{Pump Efficiency} \times 3960$

Fixed =  $(500 \times 103) \div (.86 \times 3960) = 15.1 \text{ BHP}$

Variable =  $(500 \times 103) \div (.85 \times 3960) = 11.9 \text{ BHP}$

# Building Loads

Commercial buildings use chilled water systems for cooling, and hot water systems for heating and domestic water for consumption

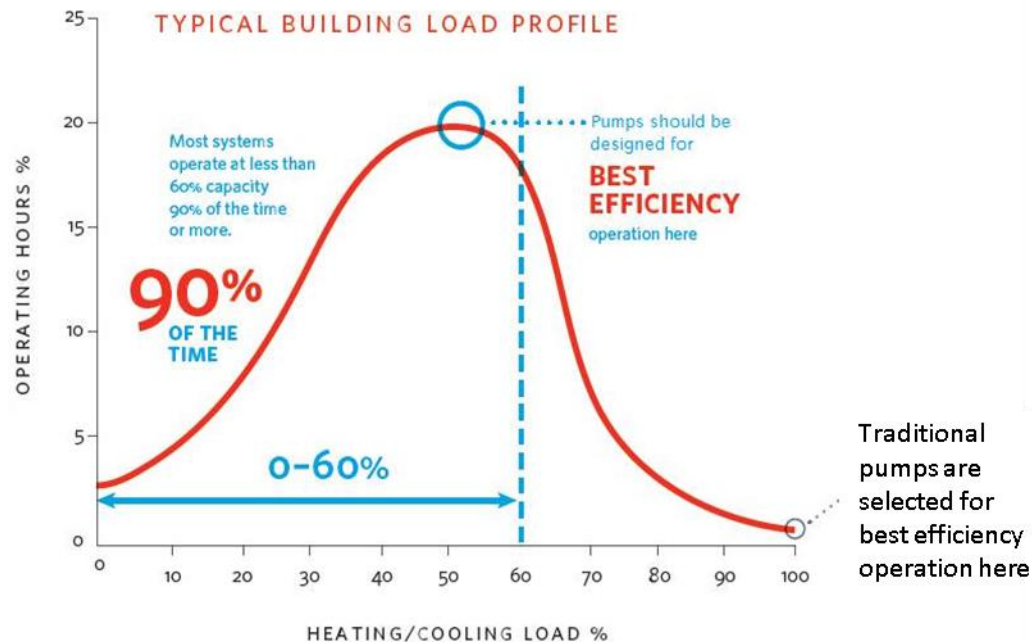
These systems operate at less than full load or part-load the vast majority of the time.

The emphasis on meeting design day heating and cooling loads results in oversized pumps.

A systems approach will typically yield a more efficient, more reliable and quieter hydronic system.

# Building Load Profile

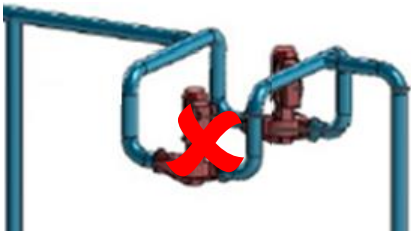
Most systems operate at less than 60% capacity, 90% of the time or more.





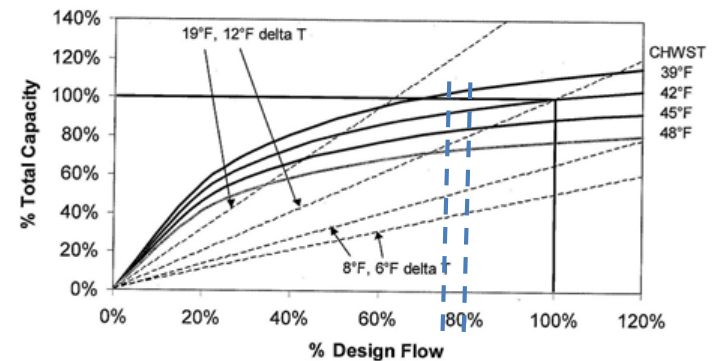
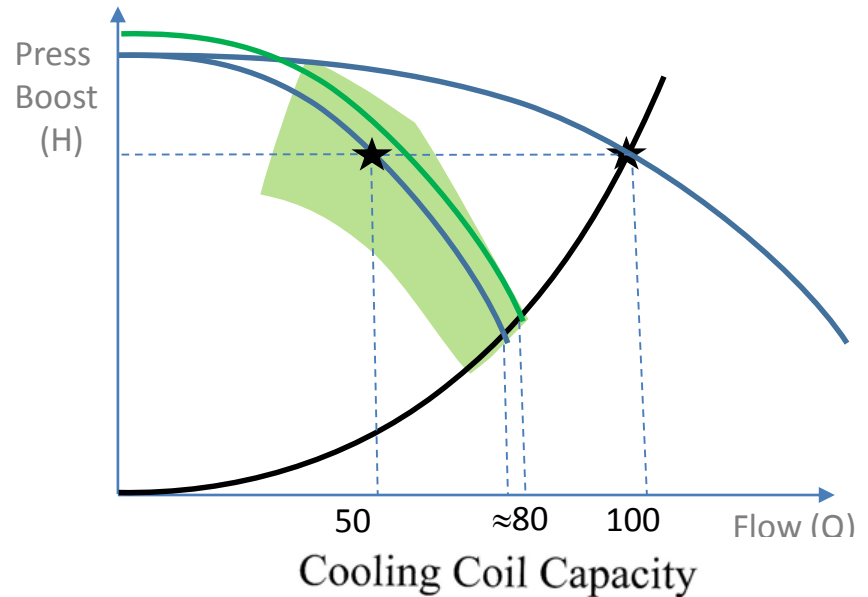
# Standby versus Redundancy

## Redundancy



Percent of Design Point heat

	80% Flow	85% Flow
45°F	85	87
42°F	95	97
41°F	98	100
40°F	101	103
39°F	104	107



# Not All Projects Require Complete Pump Replacement

## Constant Speed Pumps Retrofit What is Involved?

- Retain casing
- Install a variable speed rotating assembly (new motor/drive/impeller, adapter, flush line and seal)
- No piping changes, no new insulation and no pressure testing required!
- Has to be done by a professional



# Equipment to be Covered

- Source Equipment
  - Boilers
  - Chillers
- Cooling Towers/Economizer
- Expansion Tanks
- Air Separators
- Heat Emitters (Fan coils, AHU)
- Control Valves
- Balance Valves & Automatic Flow Limiters

# Types of Boilers

## Gas or oil fired hydronic boilers

- Non-condensing: Minimum 130°F return temp
  - Cast iron
  - Copper tube
- Condensing: Low temp high efficiency boilers
  - Stainless Steel
  - Aluminum

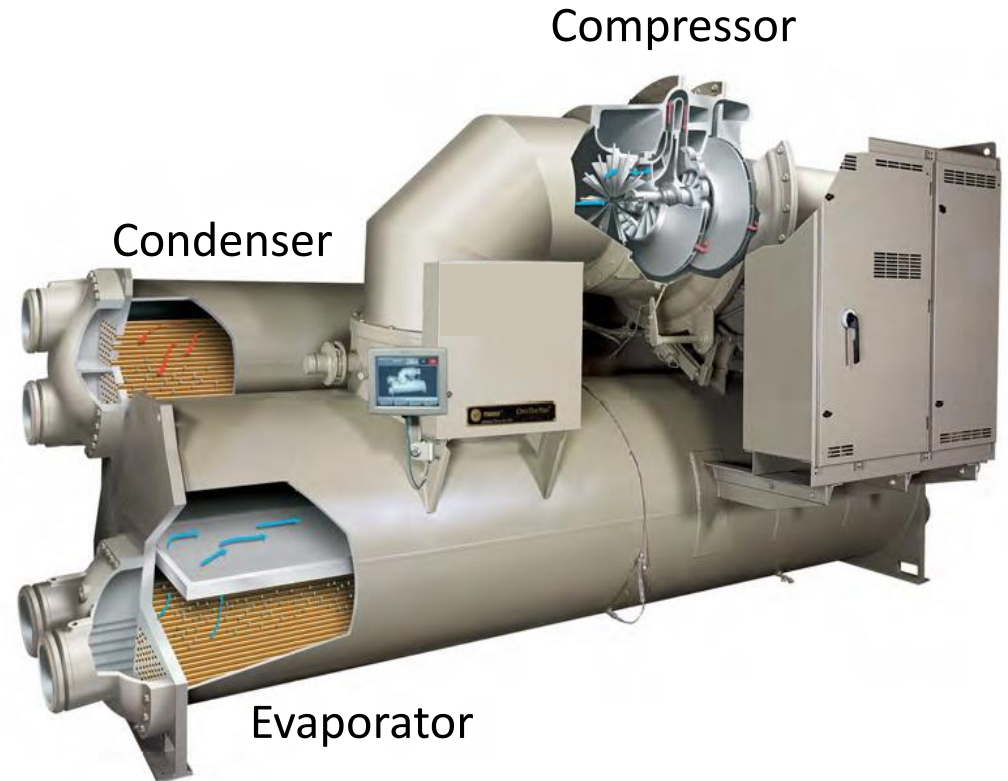
## Other Sources of Heat

- Electric boilers
- Hydronic heat pumps



# Types of Chillers

- Reciprocating
- Rotary screw
- Centrifugal (shown)
- Absorption



# Where is What Used?

## Most common

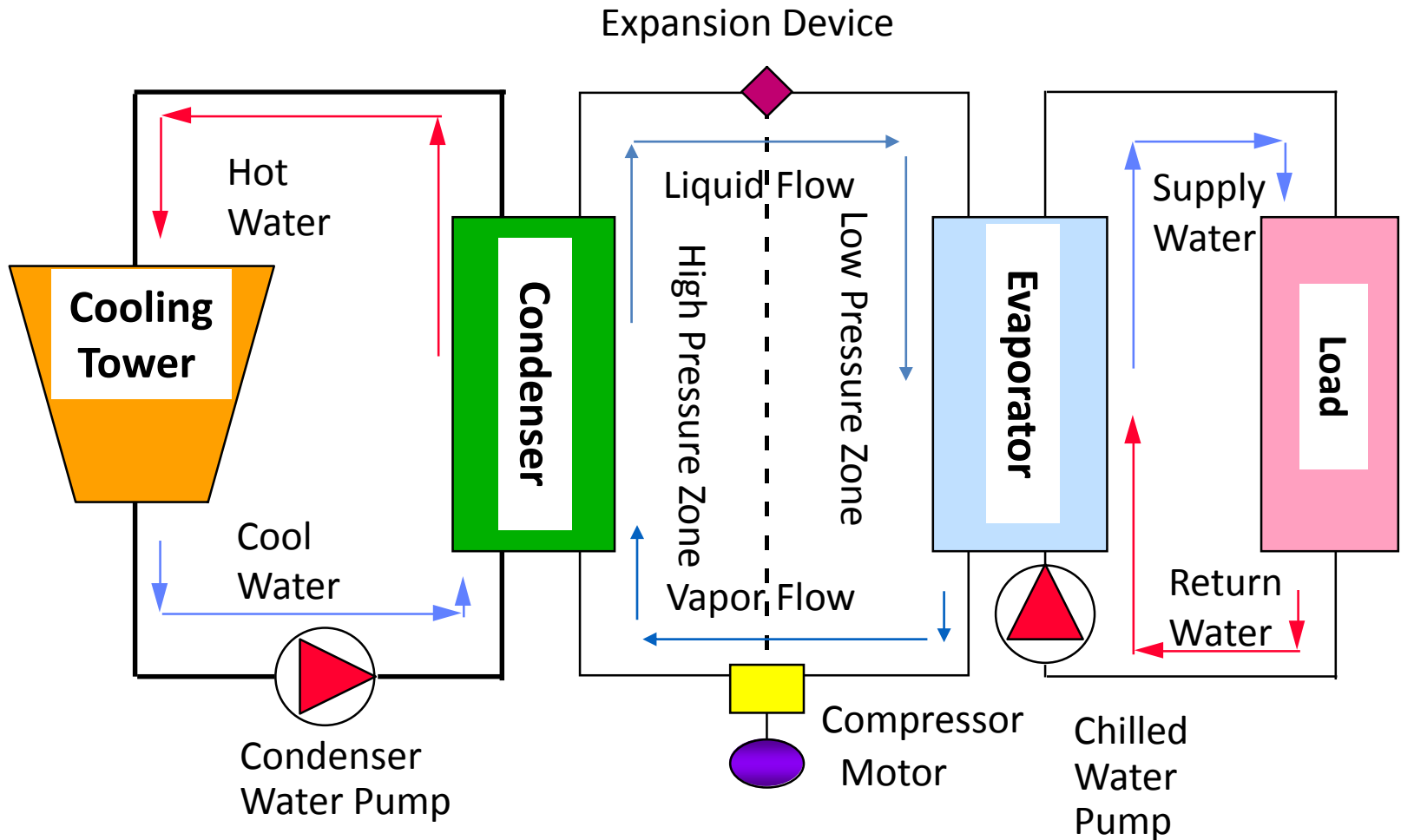
- Large chilled water plants - Centrifugal
- Mid-range size application - Rotary Screw

## Less common

- Smaller size application - Reciprocating
- Inexpensive source of steam or heat - Absorption

## Combinations of the above

# Refrigeration Cycle



# Condenser Head Pressure Control

With centrifugal chillers a minimum supply water temperature is needed to:

- Maintain optimum efficiency
- Maintain a minimum pressure differential between condenser and evaporator
- Prevent pressure imbalance



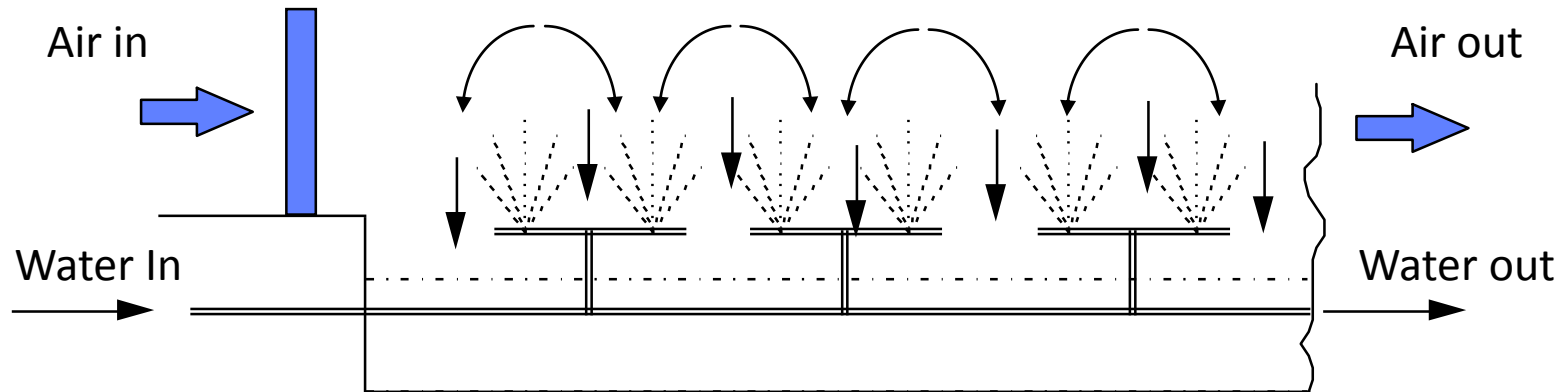
# Hermetic Compressor Guidelines

- Condenser water temperature  $> 75$  °F.
- Establish  $75$  °F within 15 minutes.
- N/O condenser water throttling valve.
- Constant condenser water flow.
- Water temperature control through fan modulation, or other methods

# Open Compressor Guidelines

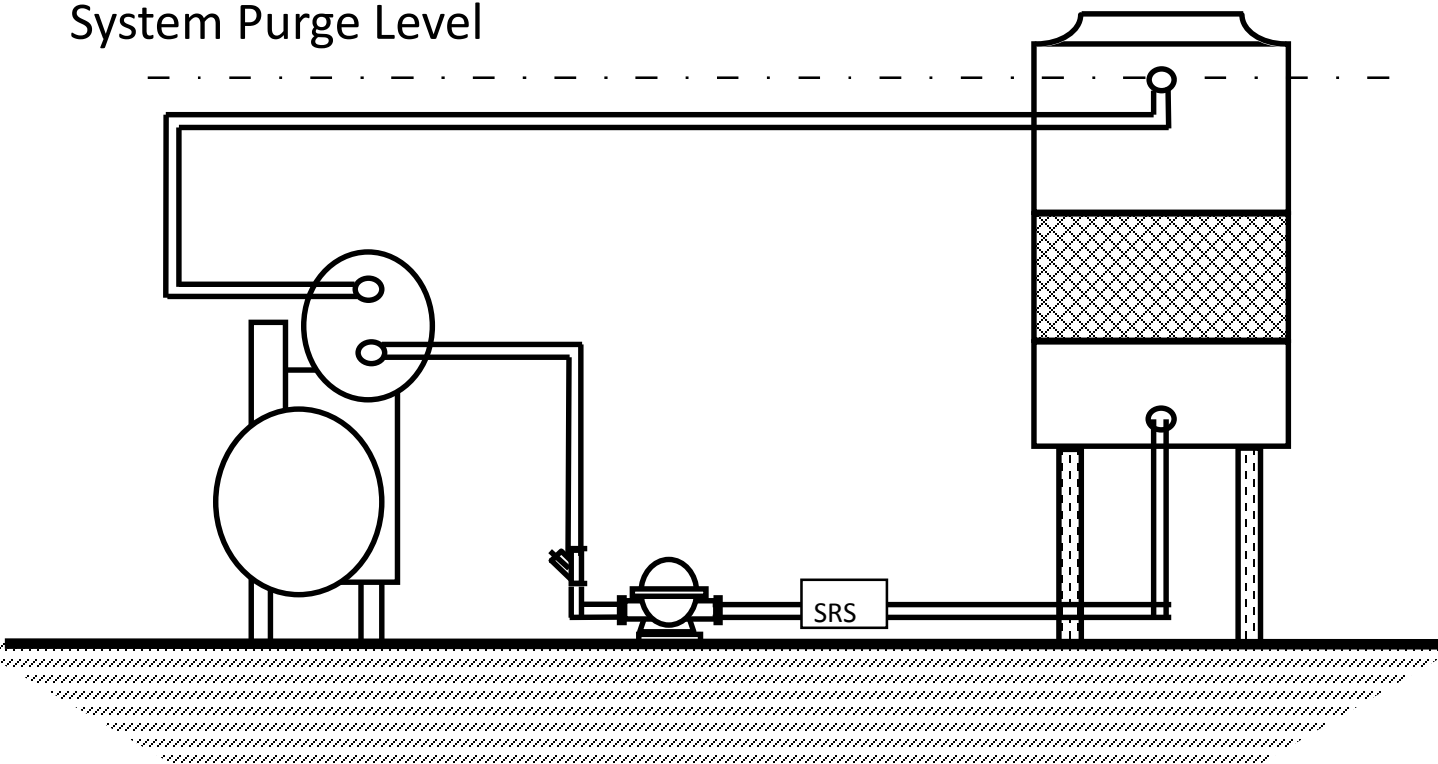
- Condenser water temperature  $> 55$  °F.
- N/O condenser water throttling valve.
- Constant condenser water flow.
- Water temperature control through fan modulation, or other methods

# Cooling Towers – Evaporative Cooler

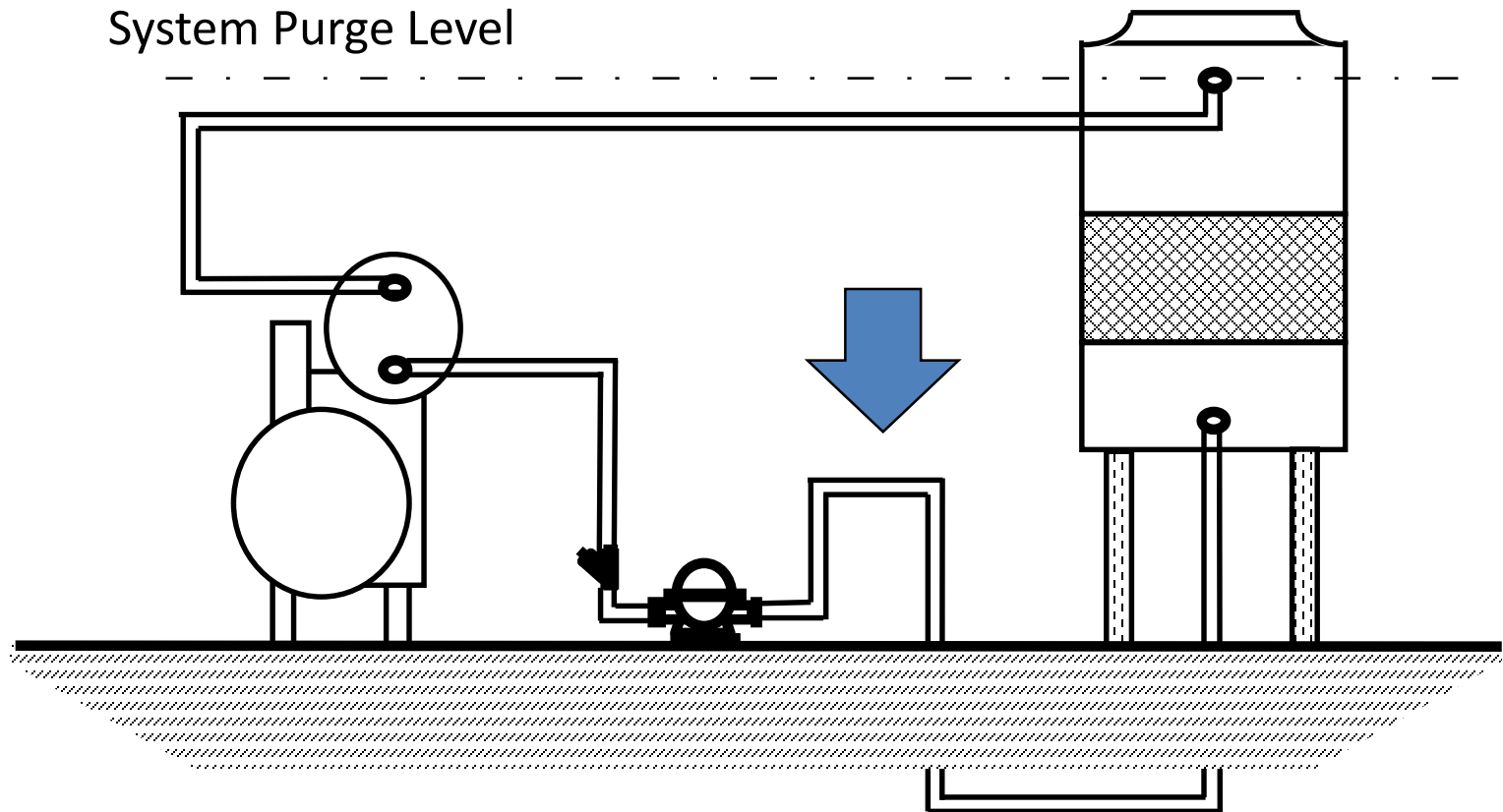


Induced Draft, Counter-flow Tower  
Forced Draft, Cross-flow Tower

# Condenser Water Piping Above Grade



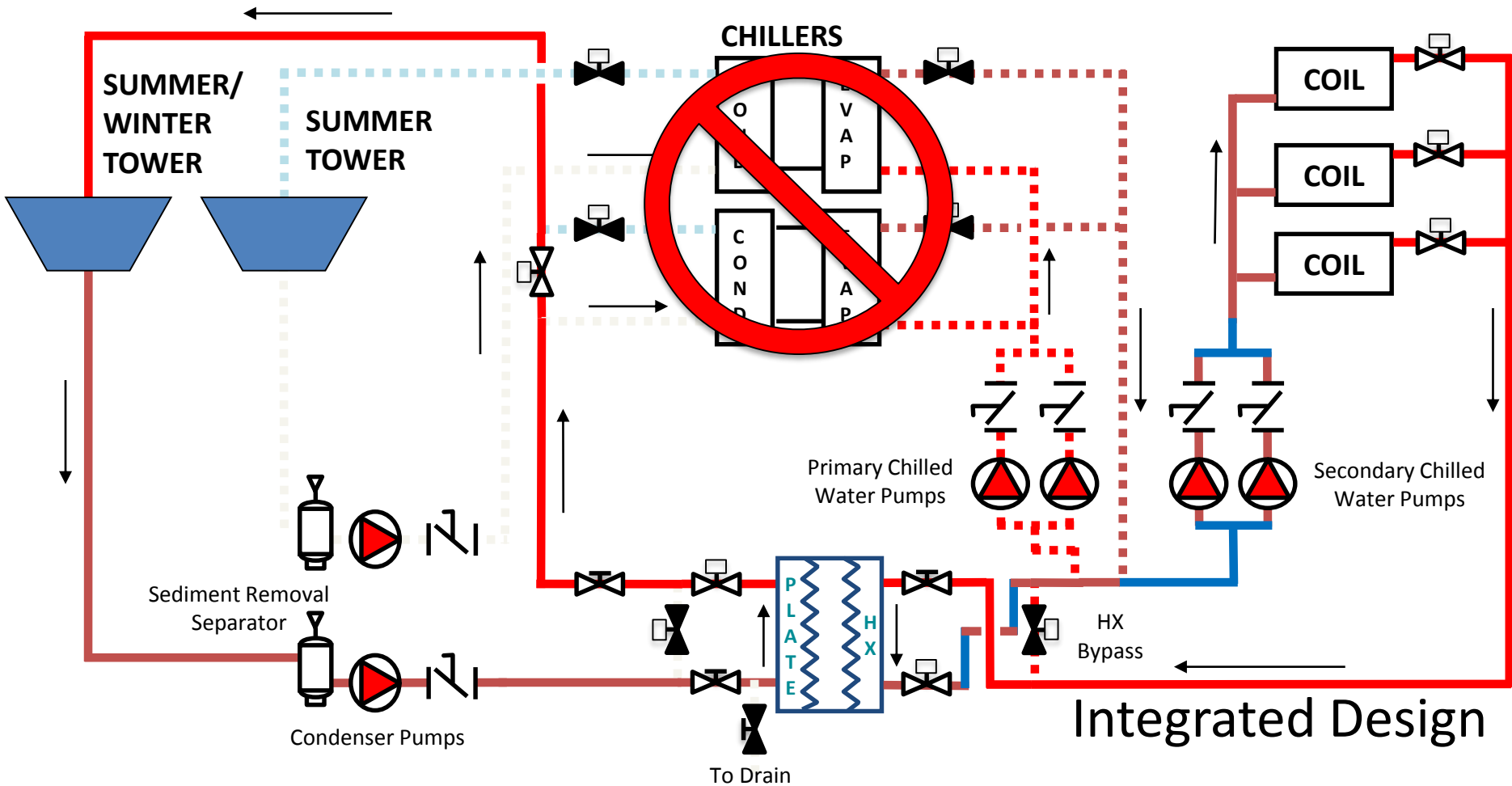
# Improper High Suction Piping



# Economizers – Goal/Definitions

- Mechanical devices intended to reduce energy consumption or to perform another useful function such as precooling a fluid.
- Airside economizers – use cool outside air directly as a means of cooling the indoor space.
- Waterside economizers – use cooled water indirectly as a means of cooling the indoor space.
- Numerous design variations of waterside economizers – typically they utilize a cooling tower and heat exchanger to indirectly cool the chilled water loop, which is used to reject heat from the building via the hydronic coils.

# 2 Identical Cooling Towers & Plate & Frame HX Winter Cycle – Chillers Off – Economizer



Integrated Design

# Economizer System Design Alternative

- **Cooling Tower and Heat Exchanger**

- Two Identical Cooling Towers

- Each Tower Sized for 50% of Summer Load

- Winter Load is less than 50% of Summer Load

- Design Considerations

- Lower first cost alternative

- Run Both Towers in Summer Mode

- Drain One Tower During Winter

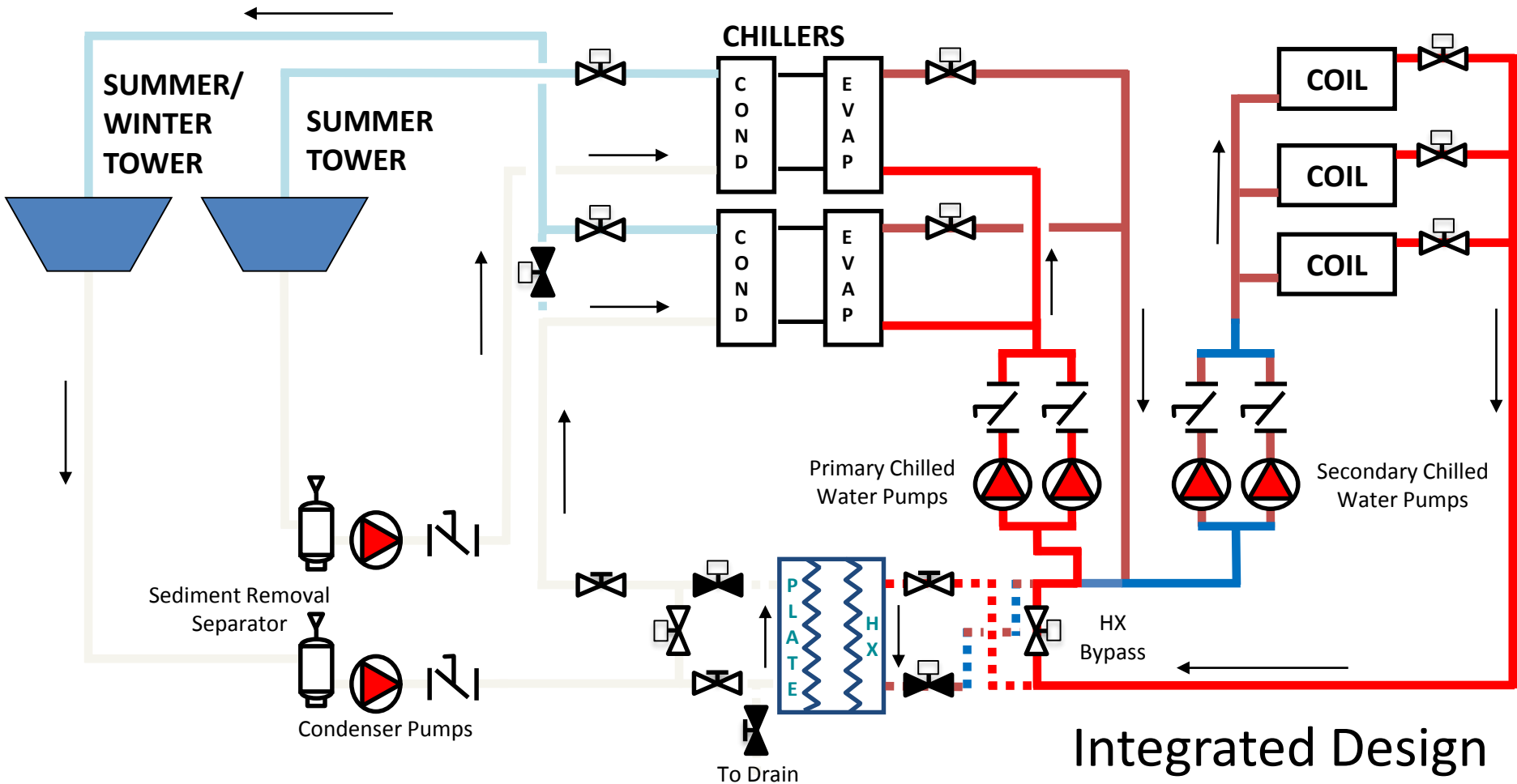
- Run Only Winter Tower in Economizer Mode

- Freeze Protection Required

- Run Both Towers when Load Shaving

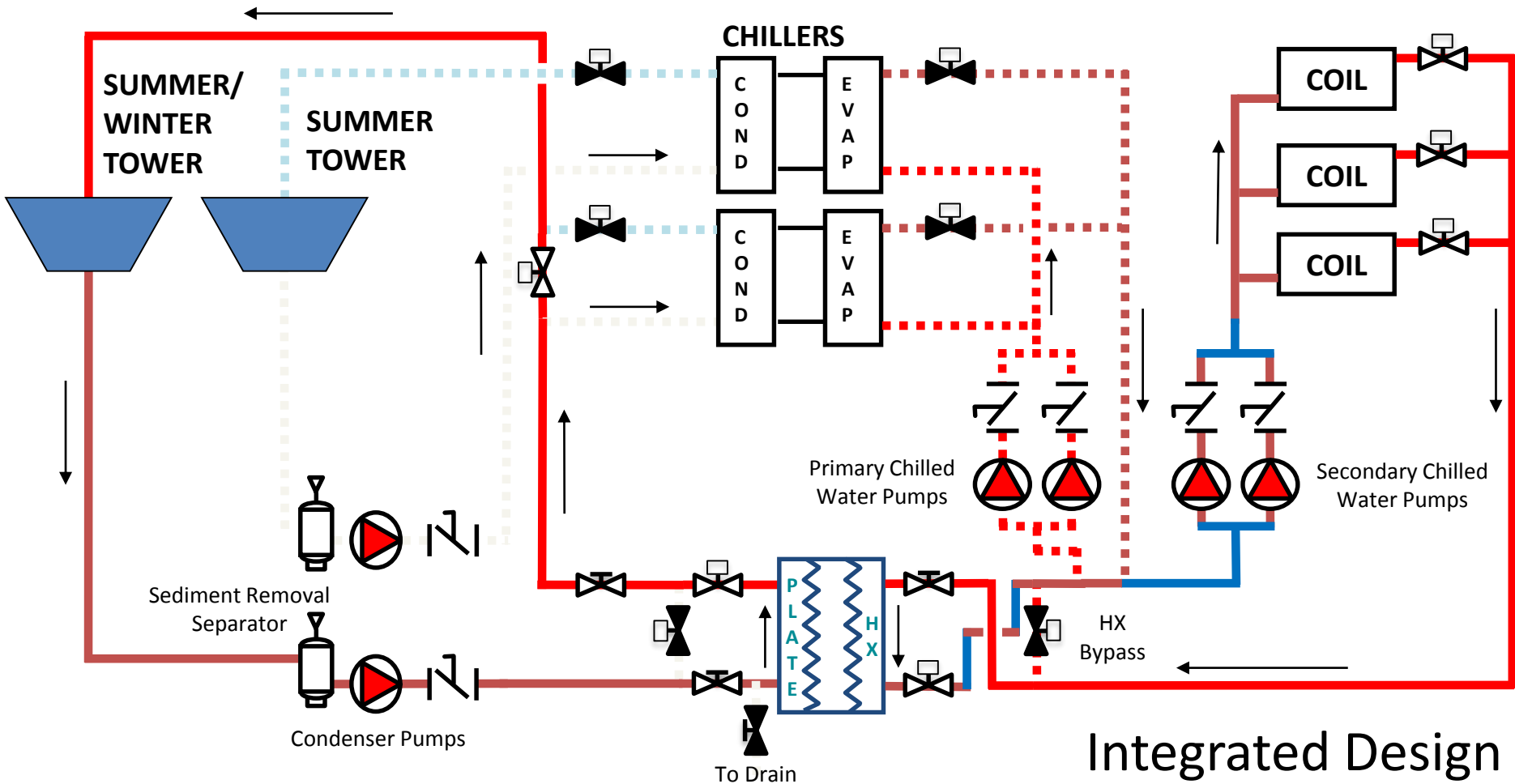


# 2 Identical Cooling Towers & Plate & Frame HX Summer Cycle – Chillers On

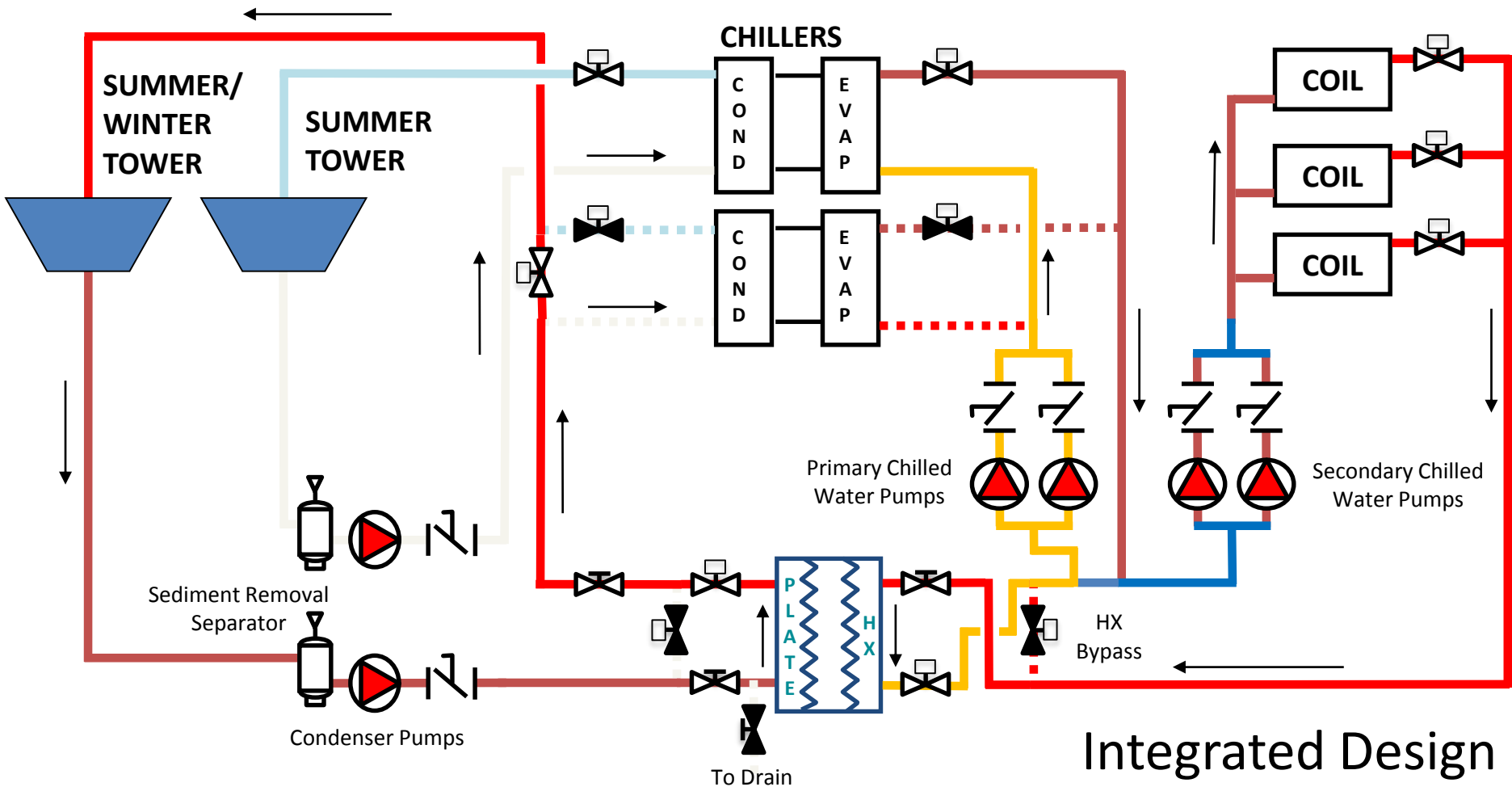


Integrated Design

# 2 Identical Cooling Towers & Plate & Frame HX Winter Cycle – Chillers Off – Economizer

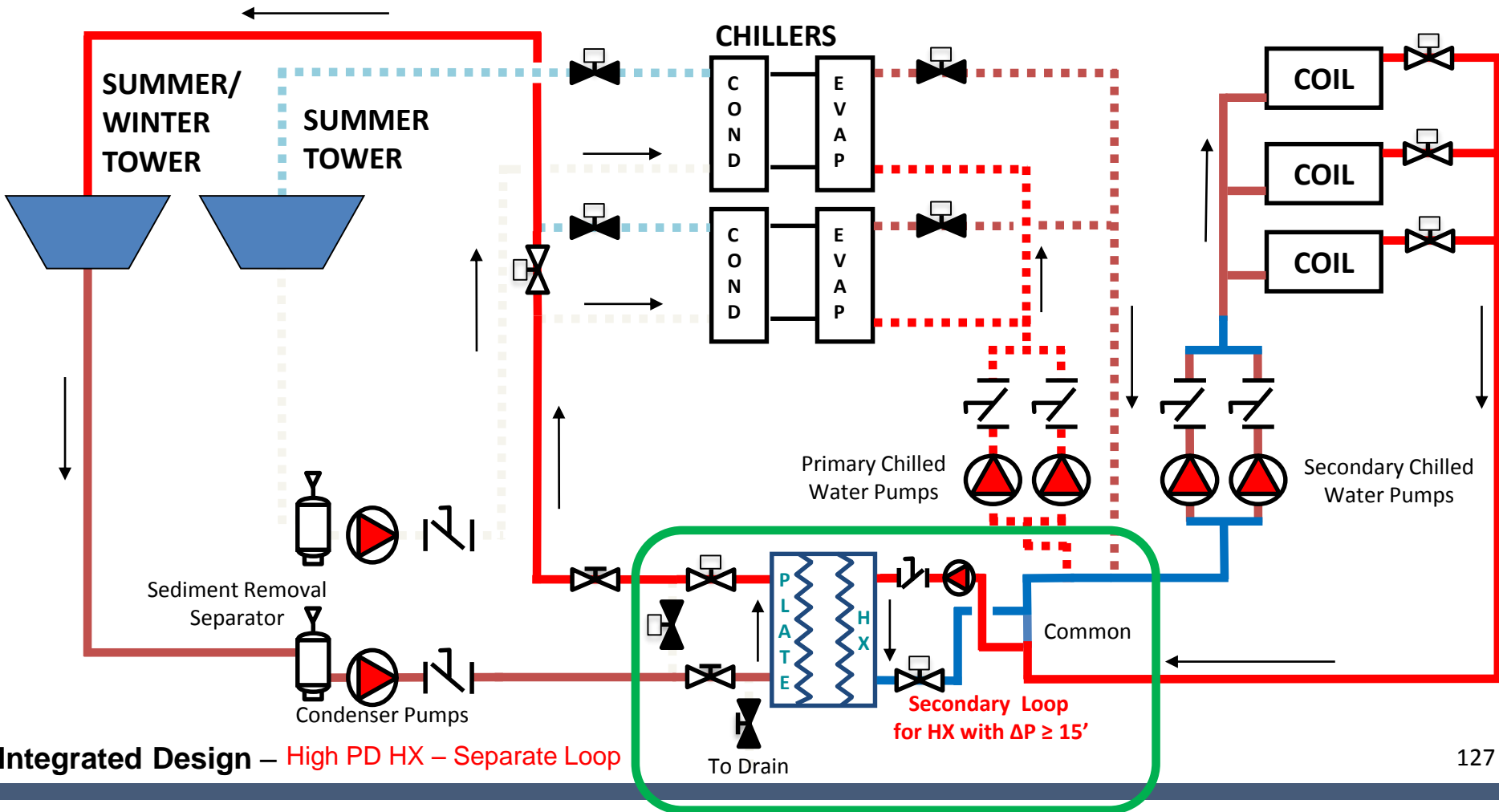


# 2 Identical Cooling Towers & Plate & Frame HX Summer Cycle – Chillers On – Load Shaving



Integrated Design

# 2 Identical Cooling Towers & Plate & Frame HX Winter Cycle – Chillers Off – Economizer



Integrated Design – High PD HX – Separate Loop

# Expansion Tanks – Hydronic Systems

- Why is a tank needed?
- Absorb system expansion due to temperature change.
- Provides minimum pressure.
  - Keep the system full
  - Vent air bubbles
  - Prevent cavitation at pump, valves
- Provide a reliable system pressure reference

# Closed Loop Requirements

- Must be able to rid the system of un-necessary air.
- Prevent loss of water, reduce need for make up and avoid water damage.
- Need to control, and limit, pressure.
  - Think of a “pressure band” with upper and lower limits.
  - Initial pressure is the lower limit.

# Pressure Reducing Valve (PRV)

Fills the system from the city water supply.  
Establishes minimum fill pressure.

Consider:

- System height above fill point
- Desired residual pressure at the
- Pump NPSHR and location
- Install near expansion tank



# Relief Valve

- Needed on boiler and chilled water side to limit system pressure.
- This is the upper limit of the “band”





# Air Management in Closed Systems

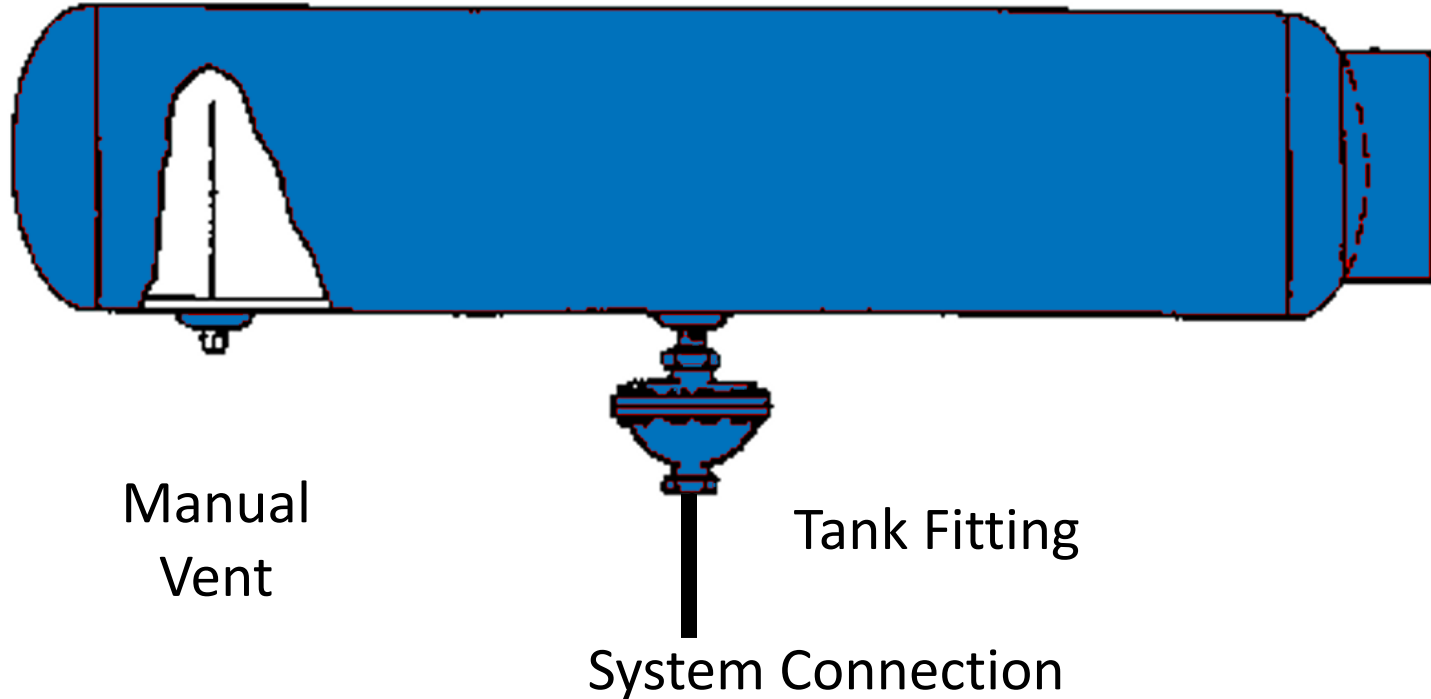
## Air Control

- Mechanical pump seal
- Standard tank
- Manual air vents
- An air separator

## Air Elimination

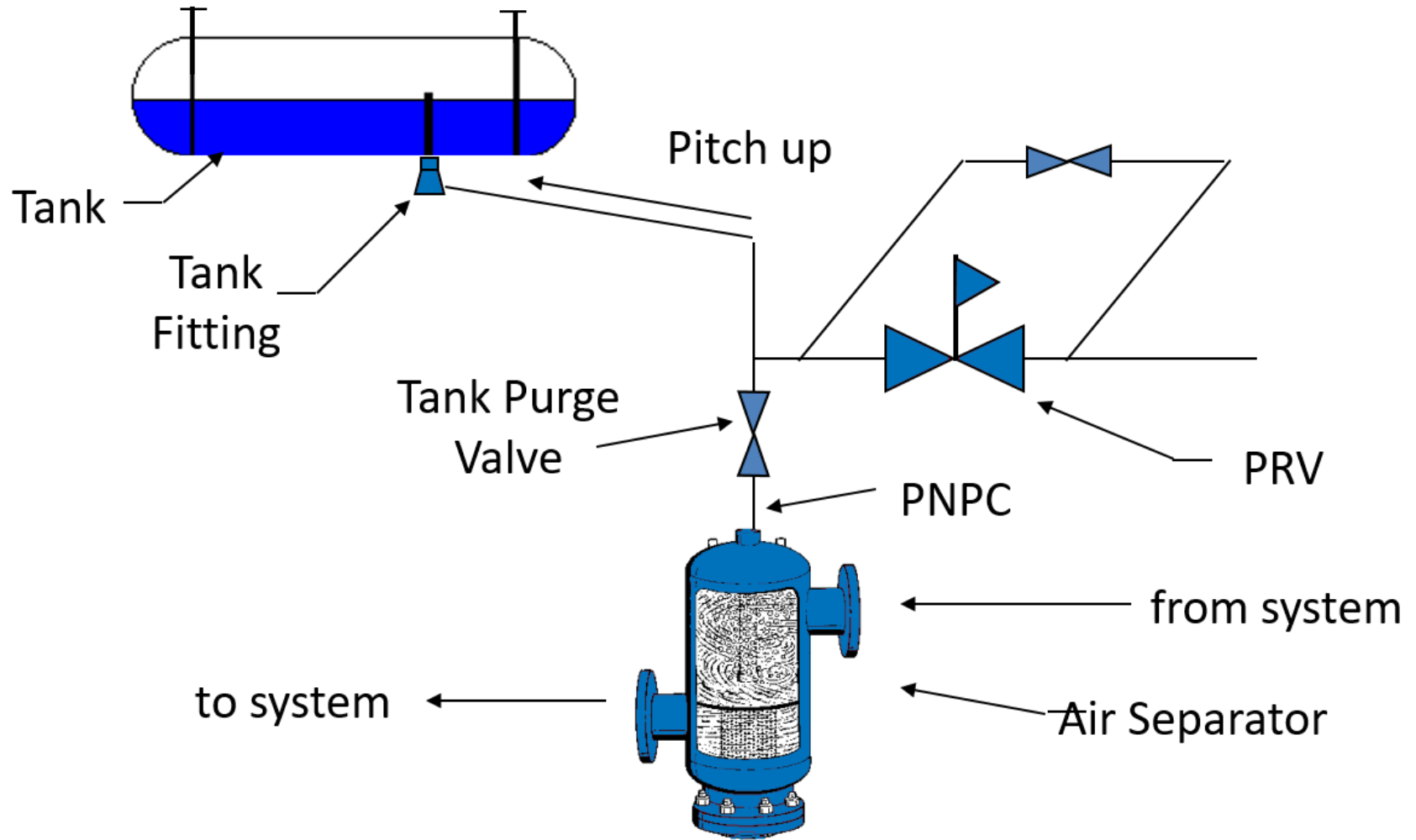
- Mechanical pump seal
- Diaphragm or bladder tank
- Automatic vents
- An air separator

# Standard Compression Tank



Used in “Air Control” strategies

# Standard Tank Installation



# Diaphragm Tank

“Acceptance volume”



Used in “Air Elimination” strategies

# Bladder Tanks



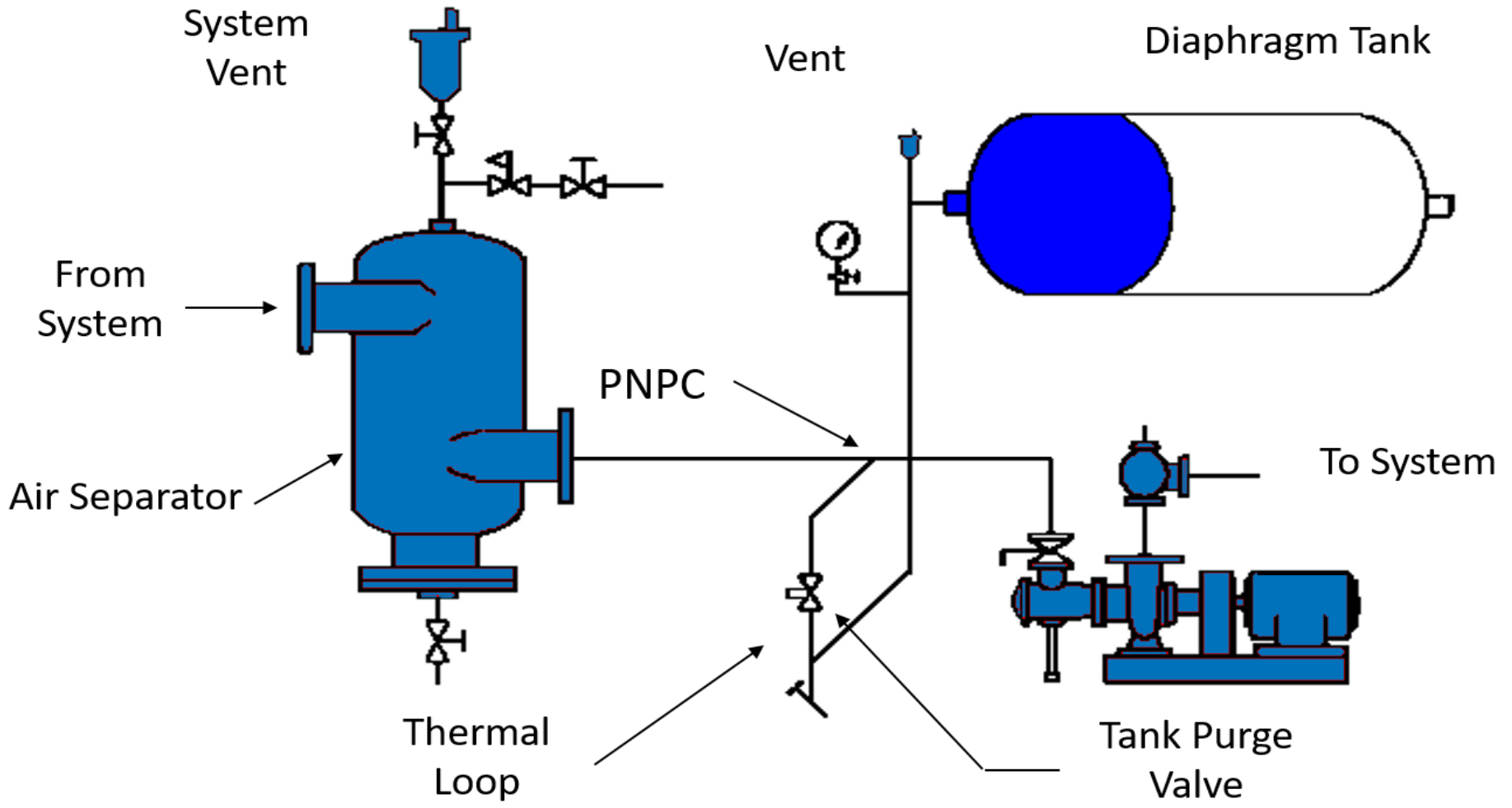
Full Acceptance



Partial Acceptance

Used in “Air Elimination” strategies

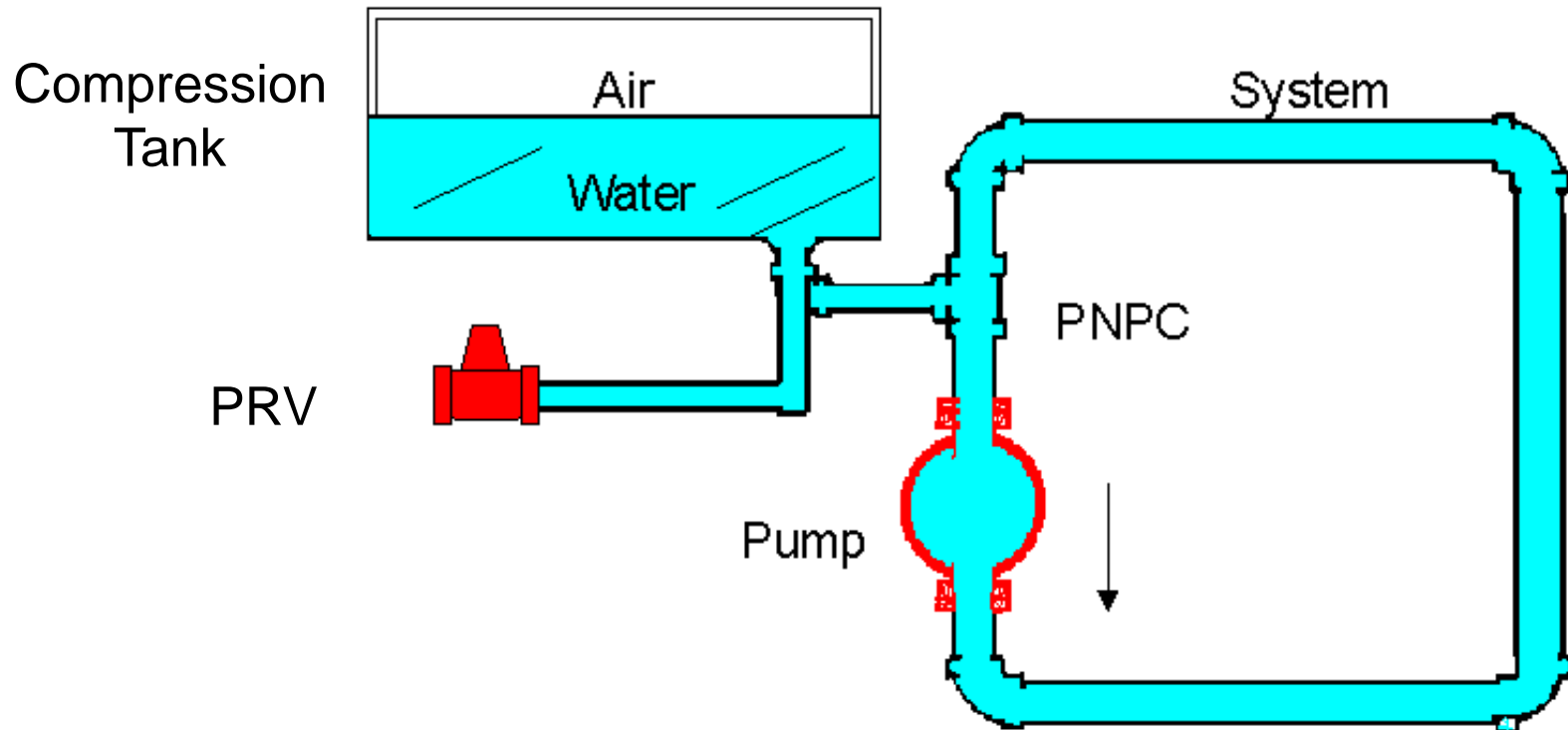
# Diaphragm Tank Installation



# Tank Sizing and Selection

- Must satisfy two conditions:
  - The volume of the tank must be large enough so that the system operates within the range of the initial fill pressure and the relief valve setting.
  - The tank's acceptance volume must be at least as large as the system's expansion volume.

# Tank Location - Installation



PNPC – Point of No Pressure Change



# Air Separators

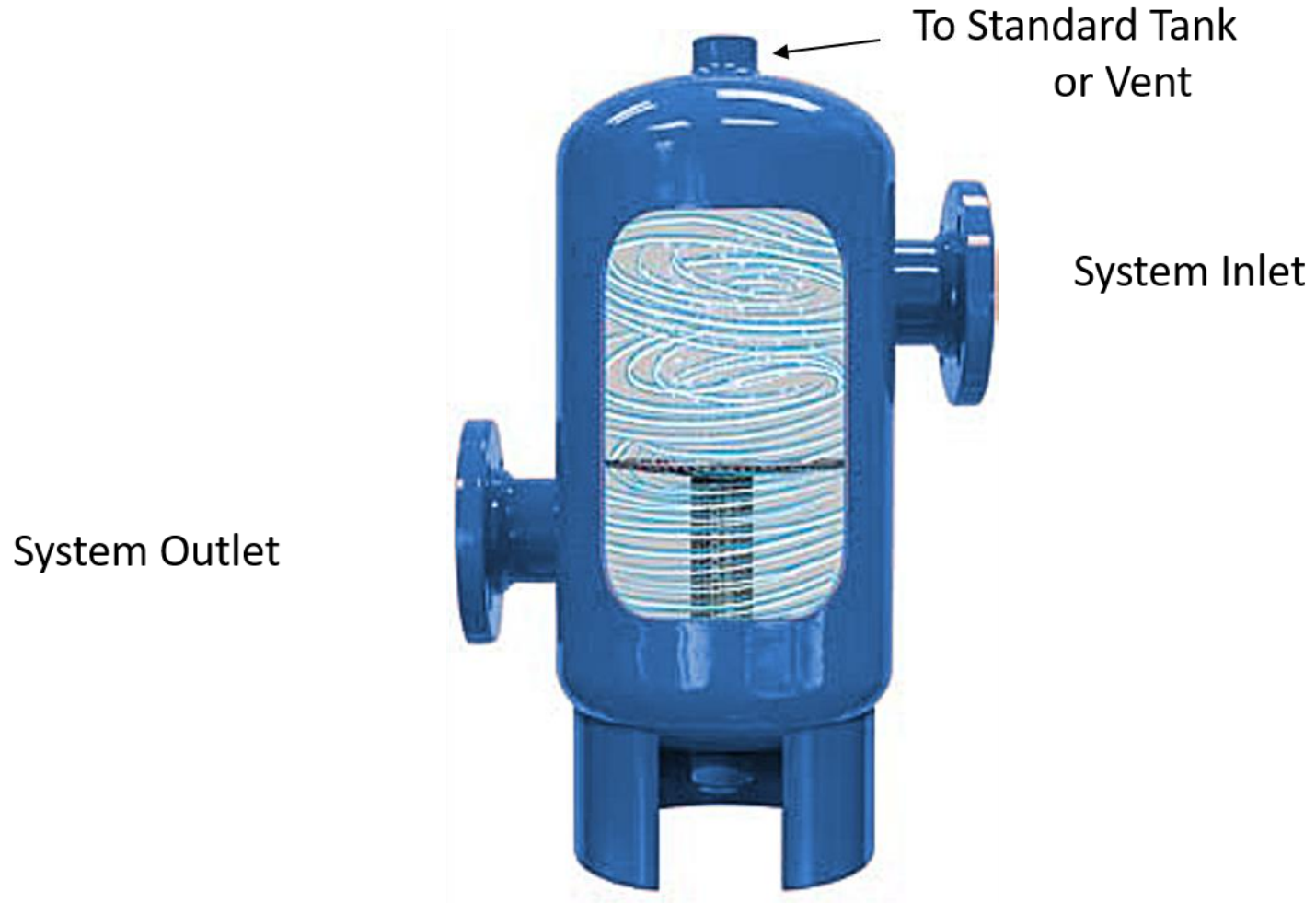
The place we want to remove air:

- Lowest Pressure
- Highest Temperature

Types of Air Separators

- Use centrifugal force
- Use coalescence

# Centrifugal Air Separator



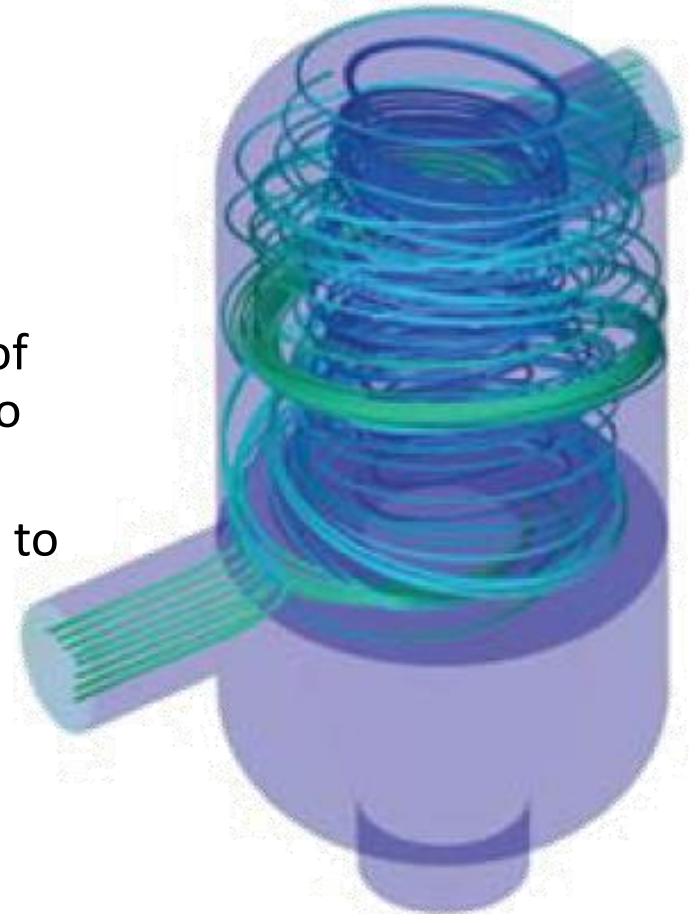
# How Does a Centrifugal Air Separator Work?

## Tangential design

- Induces centrifugal action as water enters tank
  - Heavy, air-free water forced to exterior of vessel. Lighter, air-filled water forced into center of tank
  - Separated air collects in center and rises to air vent or compression tank

## Velocity reduction

- Tank body sized 3x the inlet/outlet nozzle size
  - Allows air to come out of solution



# Coalescing Removal Separator

## Velocity Reduction

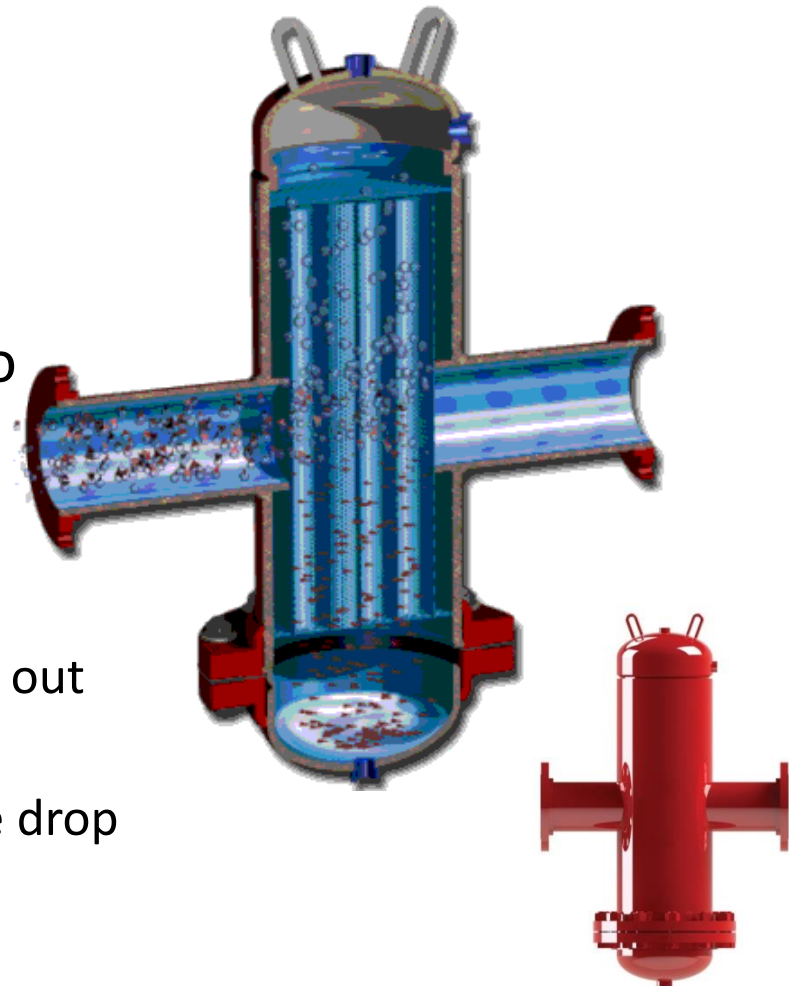
- Tank body 2x inlet/outlet nozzles

Medium inside tank provides surface area for air and sediment to “stick” to

- Medium “pulls” entrained air and sediment out of solution

## Low inlet velocity critical

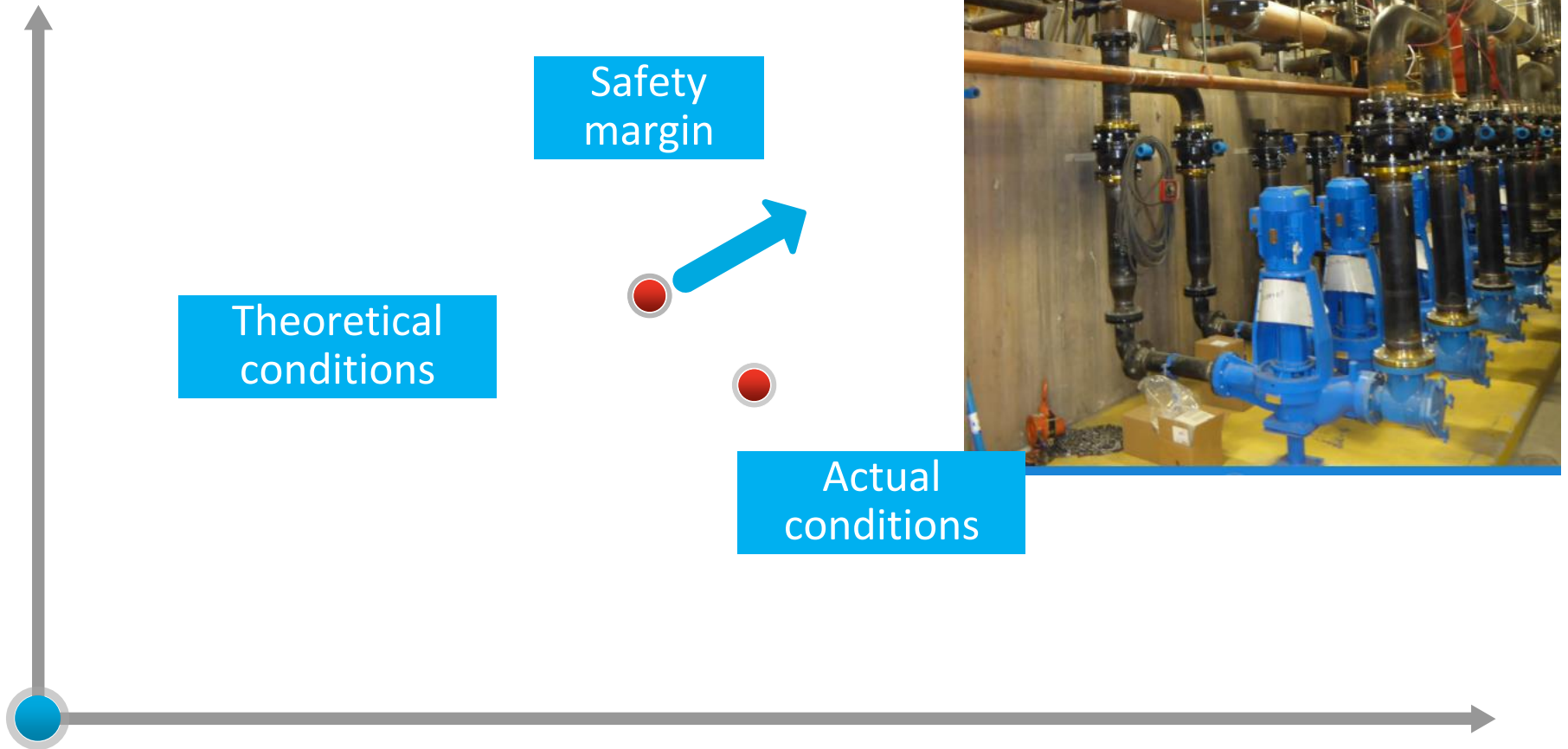
- Low fluid speed necessary to “pull” air out of solution
- Coalescing medium increases pressure drop



# Fan Coils



# Life Cycle Concerns – Design Risk



# Traditional Pump Selection Energy Savings

	Traditional selection (left of BEP):	Operating point at 50% design flow:
Duty	1250gpm at 70ft	625gpm at 38.5ft
	79.1%	67.1%
Power	27.9 bhp	9.06 bhp

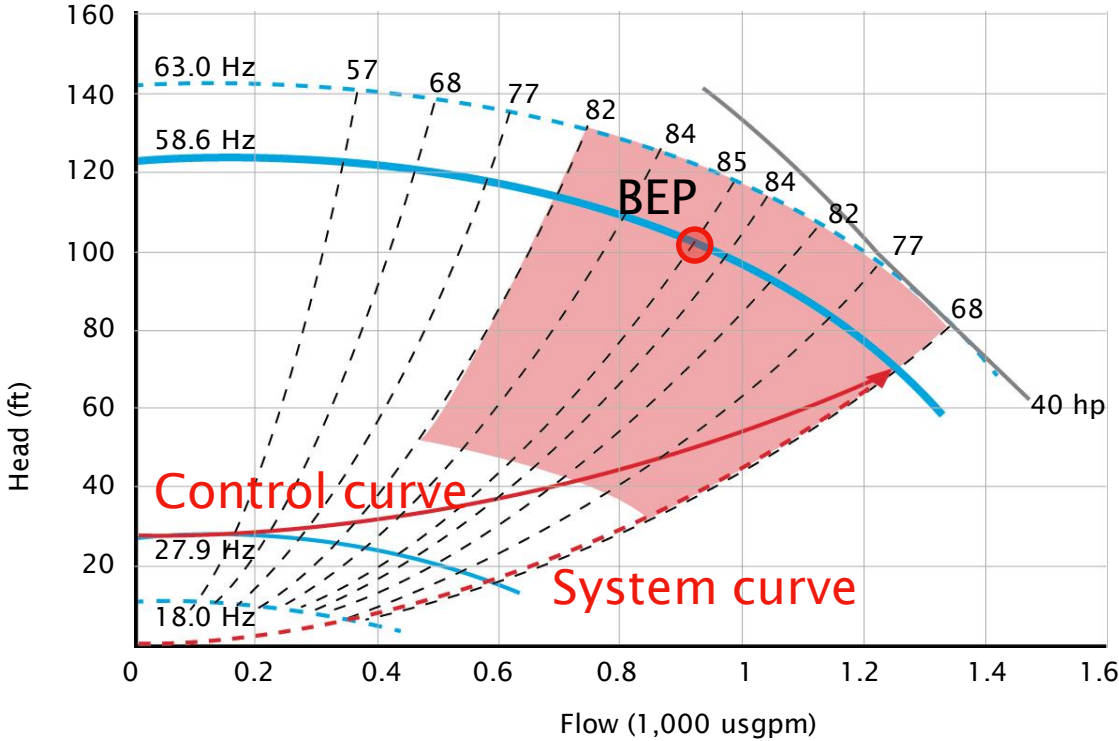
Efficiency

**67.5%**

**ENERGY  
SAVINGS**

Below  
**ASHRAE 90.1  
requirements!**

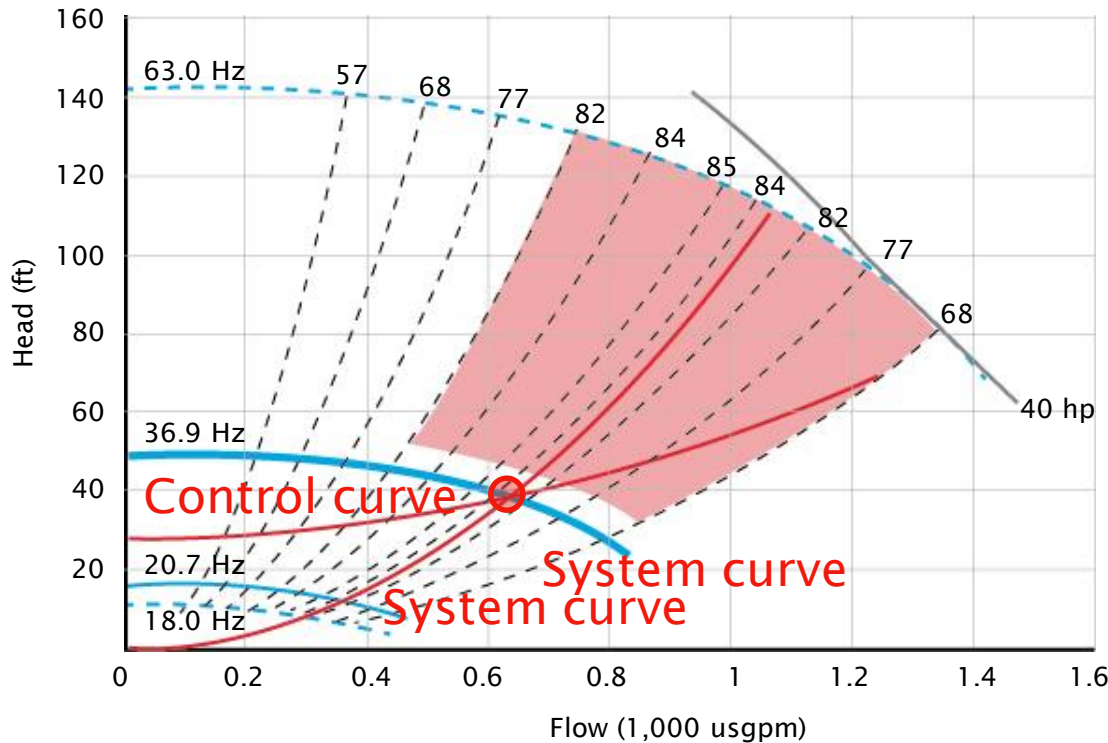
# Pump Selection



- Selection to right of BEP
- 1250gpm at 70ft
- 68.1% efficiency
- 32.5bhp



# Pump Selection at 50% Flow



- 625gpm at 38.5ft
- 83.2% efficiency
- 7.31bhp

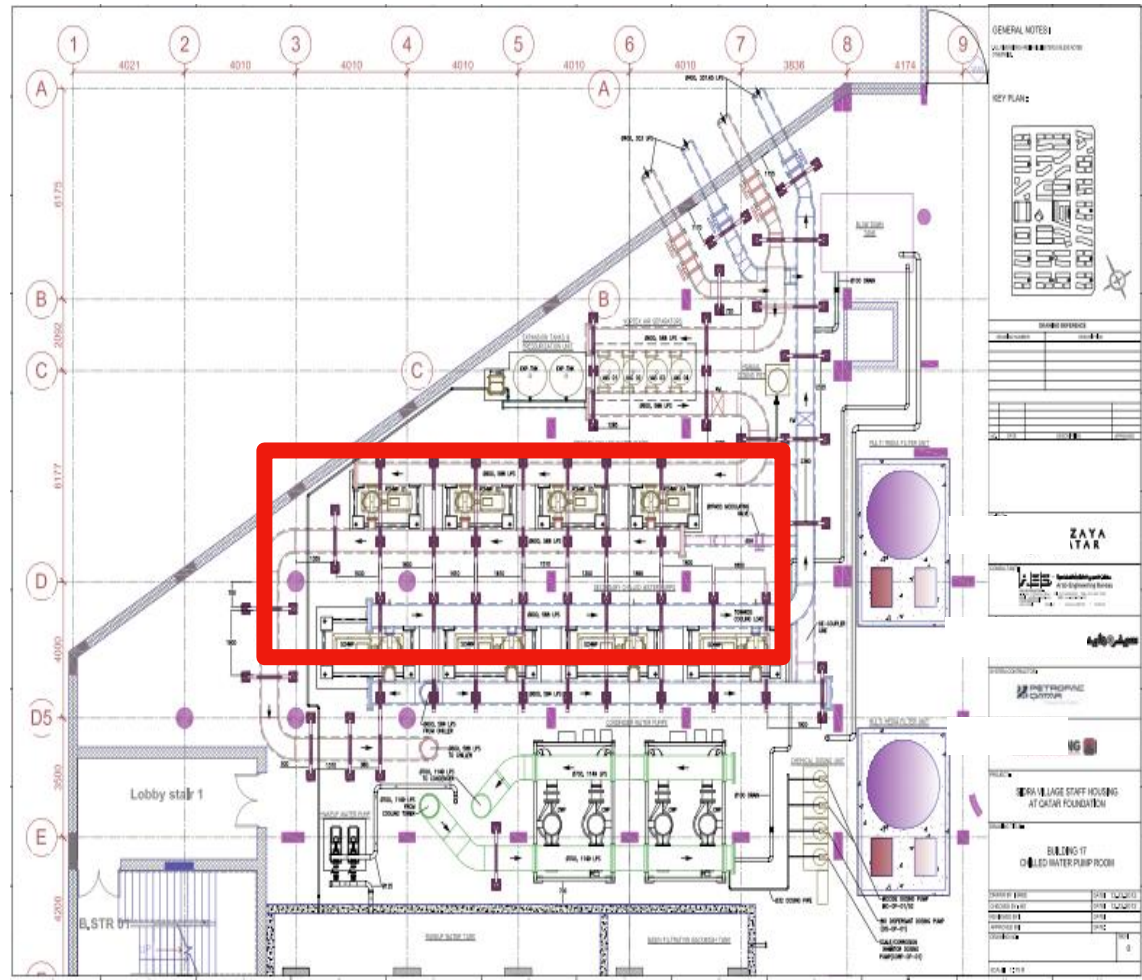
# Pump Selection Energy Savings

	Pump selection:	Operating point at 50% design flow:
Duty	1250gpm at 70ft	625gpm at 38.5ft
Efficiency	68.1%	83.2%
Power	32.5bhp	7.31bhp

**77.5%**  
**ENERGY  
SAVINGS**

Exceeds  
**ASHRAE 90.1  
requirements!**

# Installed Cost - Space



# Installed Cost – Ancillaries and Accessories



Coupling re-alignment

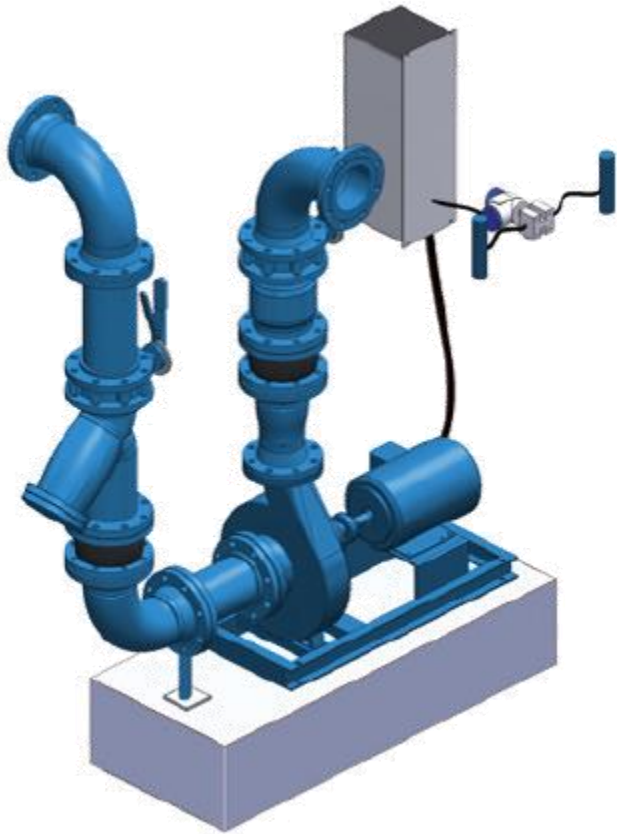
Grouting

Inertia pad

Concrete base

Flex connectors

# Installed Cost – Ancillaries and Accessories



VFD Mounting and Wiring

Sensor Acquisition and Installation

Harmonic and RFI Filtering

Thermistors and Space Heaters

Energy and Flow Metering

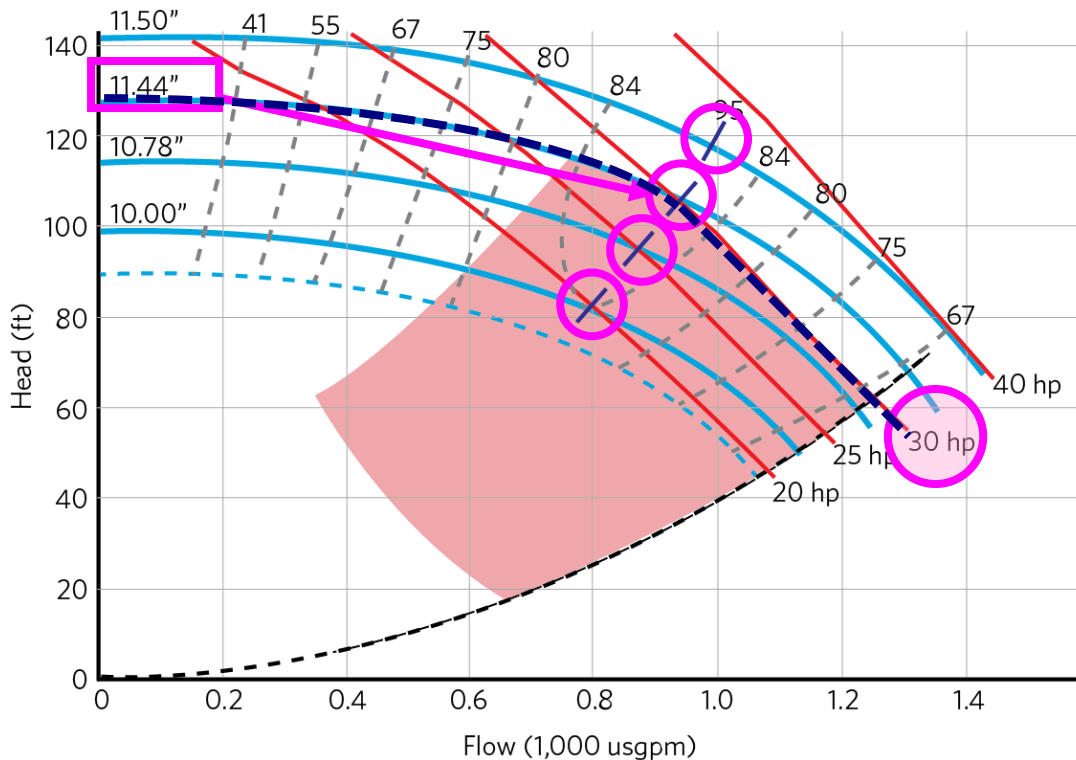
# Other Life Cycle Concerns – Reliability and Maintenance



This is often a lower specification and buying priority

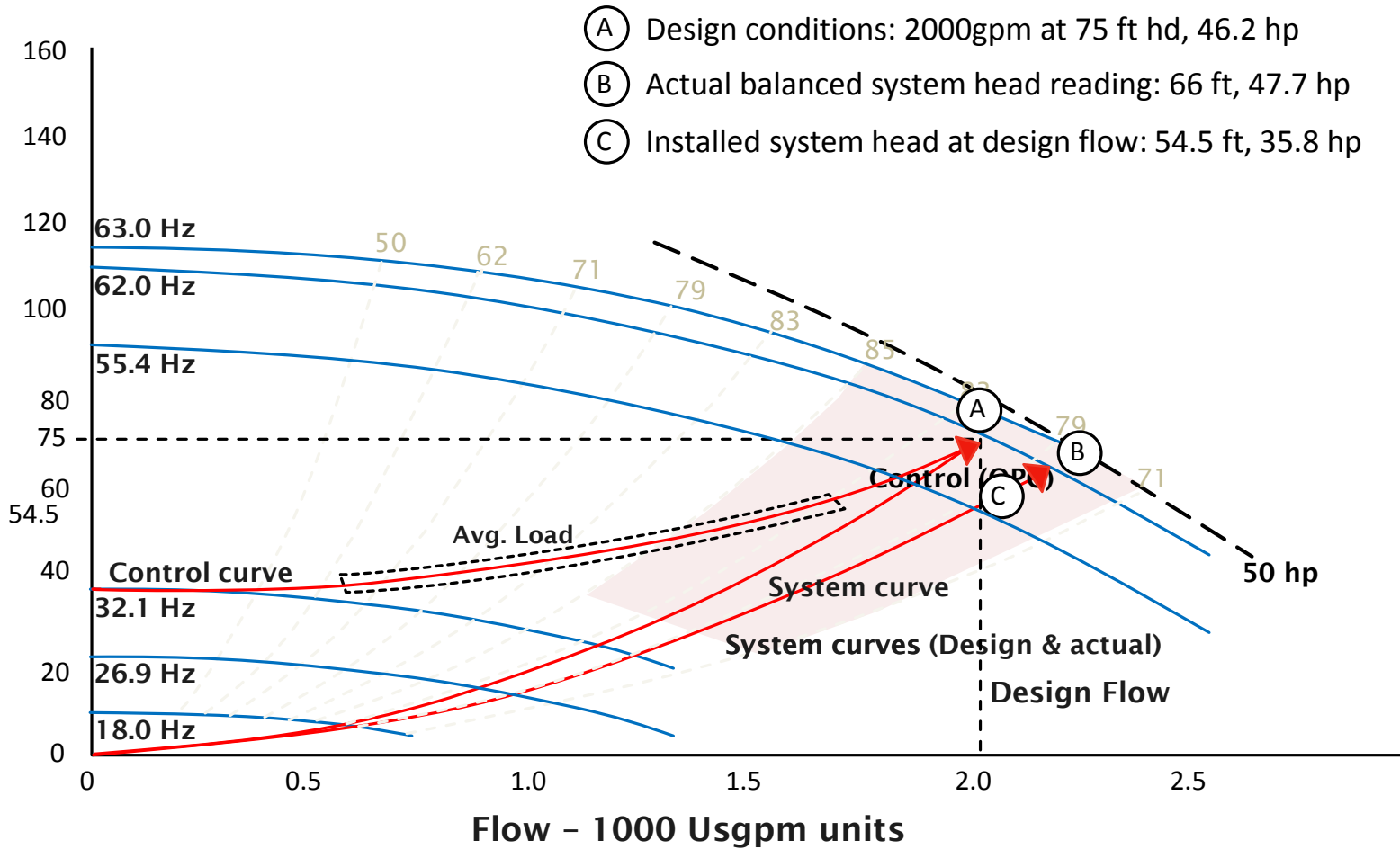
# Optimized Capacity and Motor Power

- Impeller trim is optimized to the motor power
- Electronic load limiting ensures that motor power is not exceeded



Motor sizing optimized to  
BEP – no oversized motors

# Other Life Cycle Concerns – Ease of Commissioning

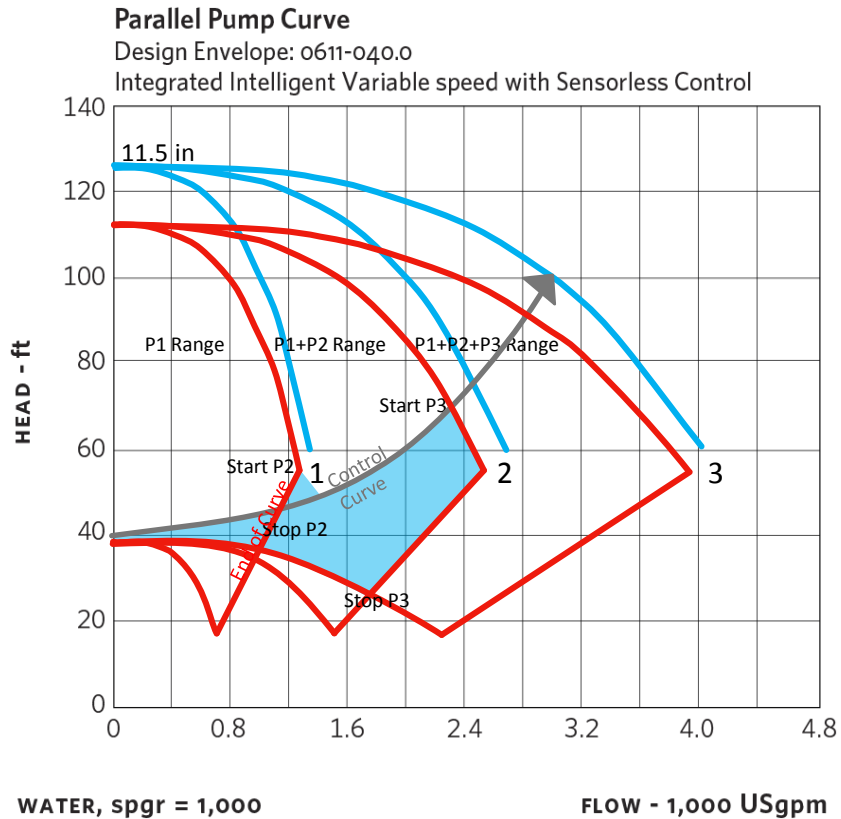


Required adjustments are often impractical or delayed, resulting in wasted energy saving opportunities



# BMS Parallel Control

## 3-pump variable speed curves

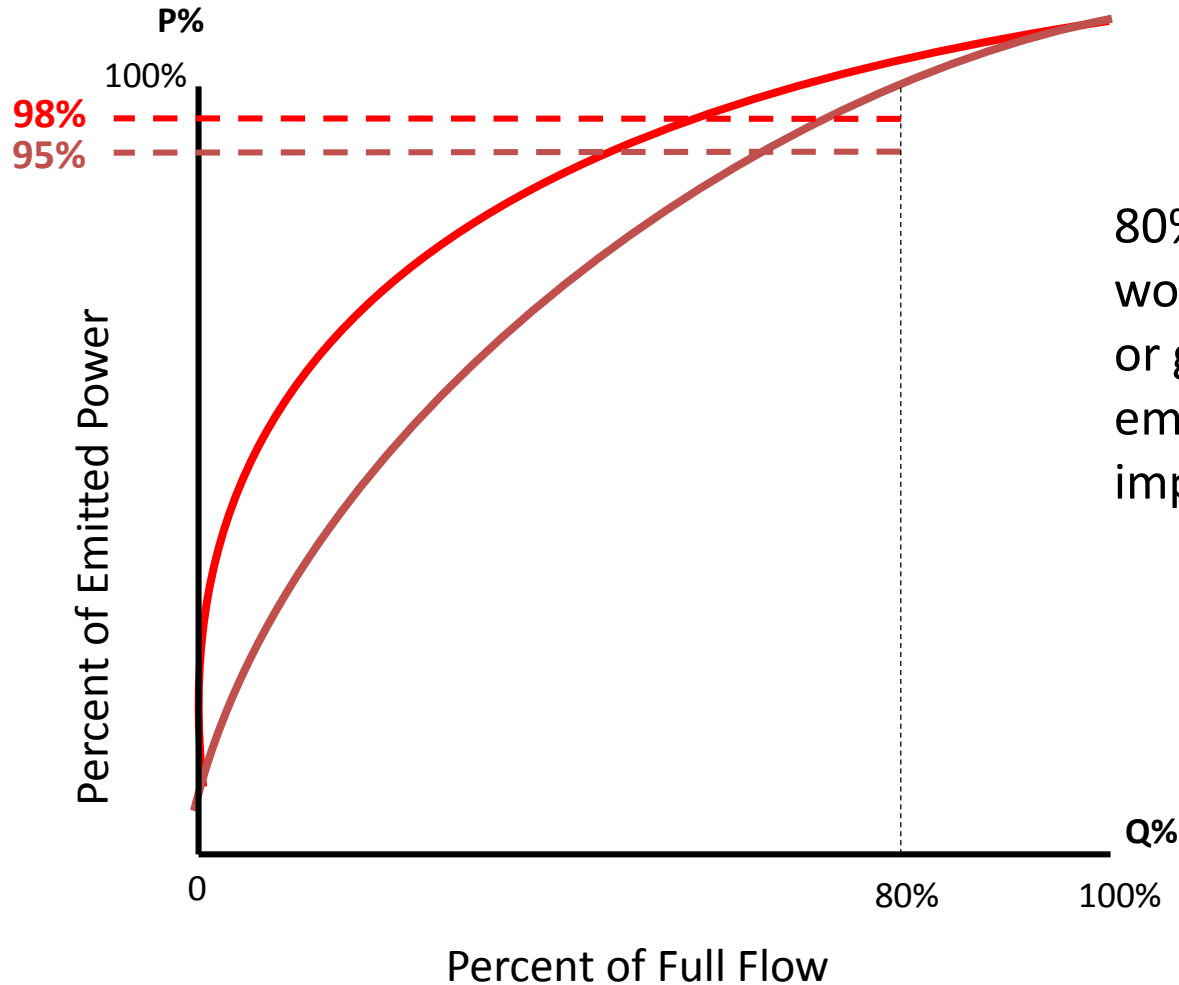


# Benefits of parallel operation versus traditional BMS parallel pump control

- Energy savings
- Typical 3-pump variable flow system / 50% average load / 40hp mtrs
- BMS operating cost\* ~ \$30, 371
- Parallel Sensorless Pump Control operating cost\* ~ \$20,092
- 72.5 metric tons CO<sub>2</sub> or equivalent
- Parallel Sensorless pump control saved **34%** energy costs

\*Based on \$0.10/kWh – 12-months operation – 40% design head min pressure

# Redundancy - Impact on Heating or Cooling Output



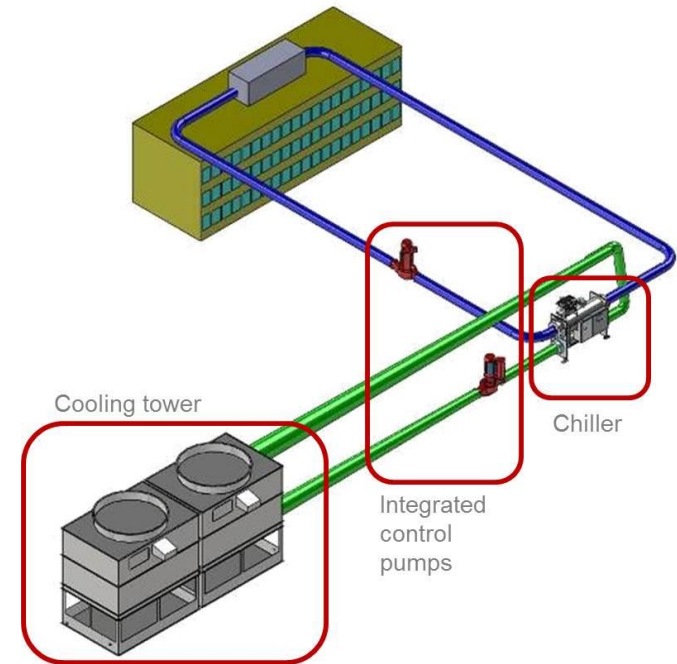
80% Capacity on a design day would still result in approx. 95% or greater heating / cooling coil emission resulting in minimal impact to occupant comfort!

# Energy Savings: Chiller and Cooling Tower

Using an all-variable plant:

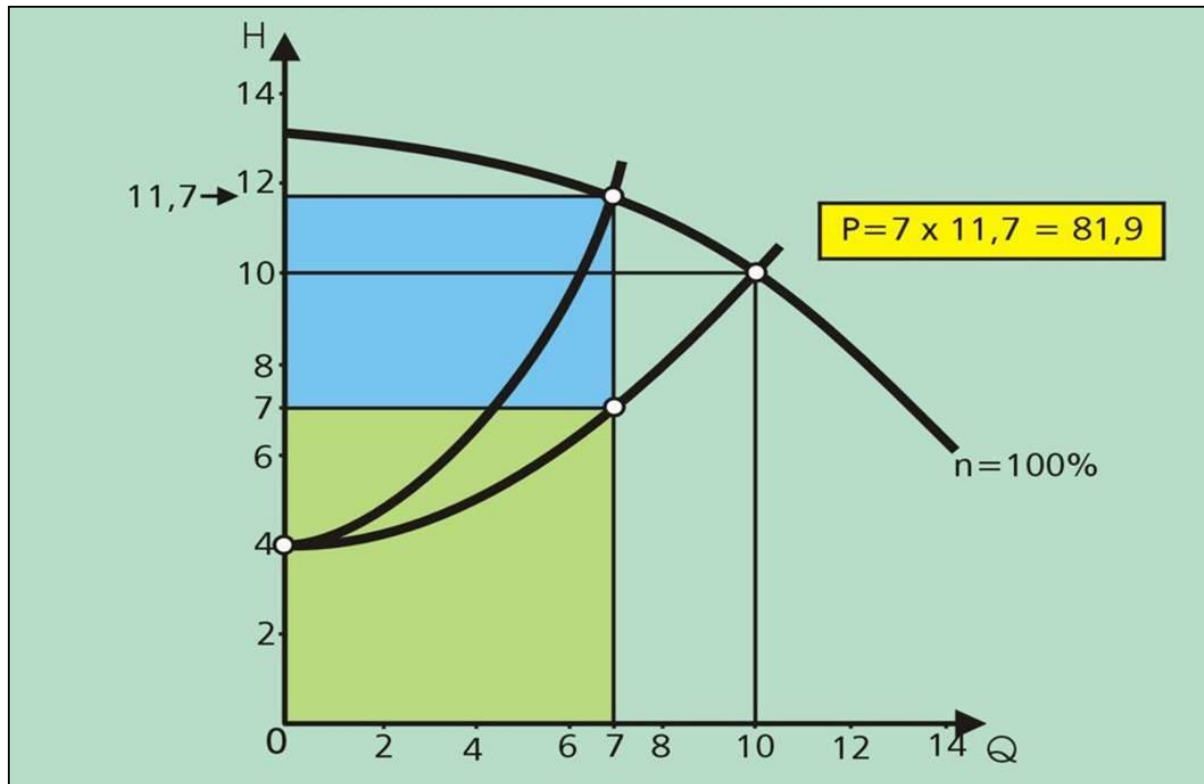
- lowers the chiller's condenser pressure requirement
- lowers the chiller's energy consumption
- enables higher tower performance
- enables better system efficiency through improved balancing of air and water flow ratios

Integrated control pumps can be used with ultra-high-efficiency plant controllers to provide energy savings.



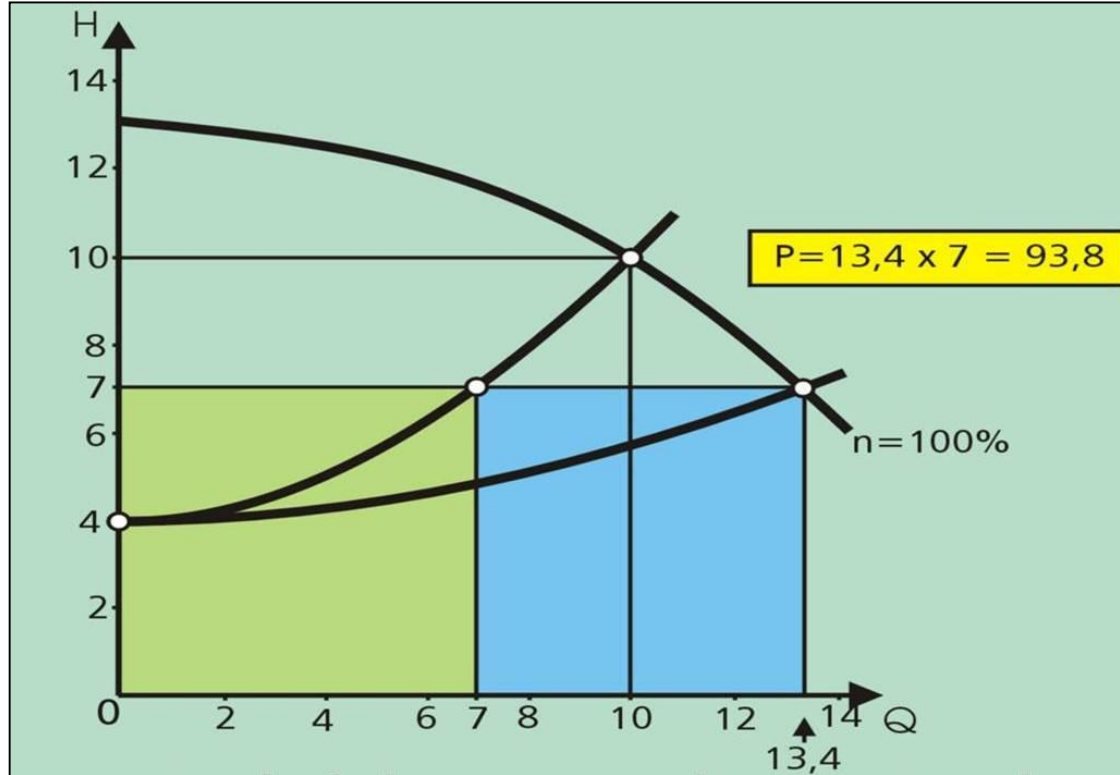
# Flow Control & DHW

# Throttle Control



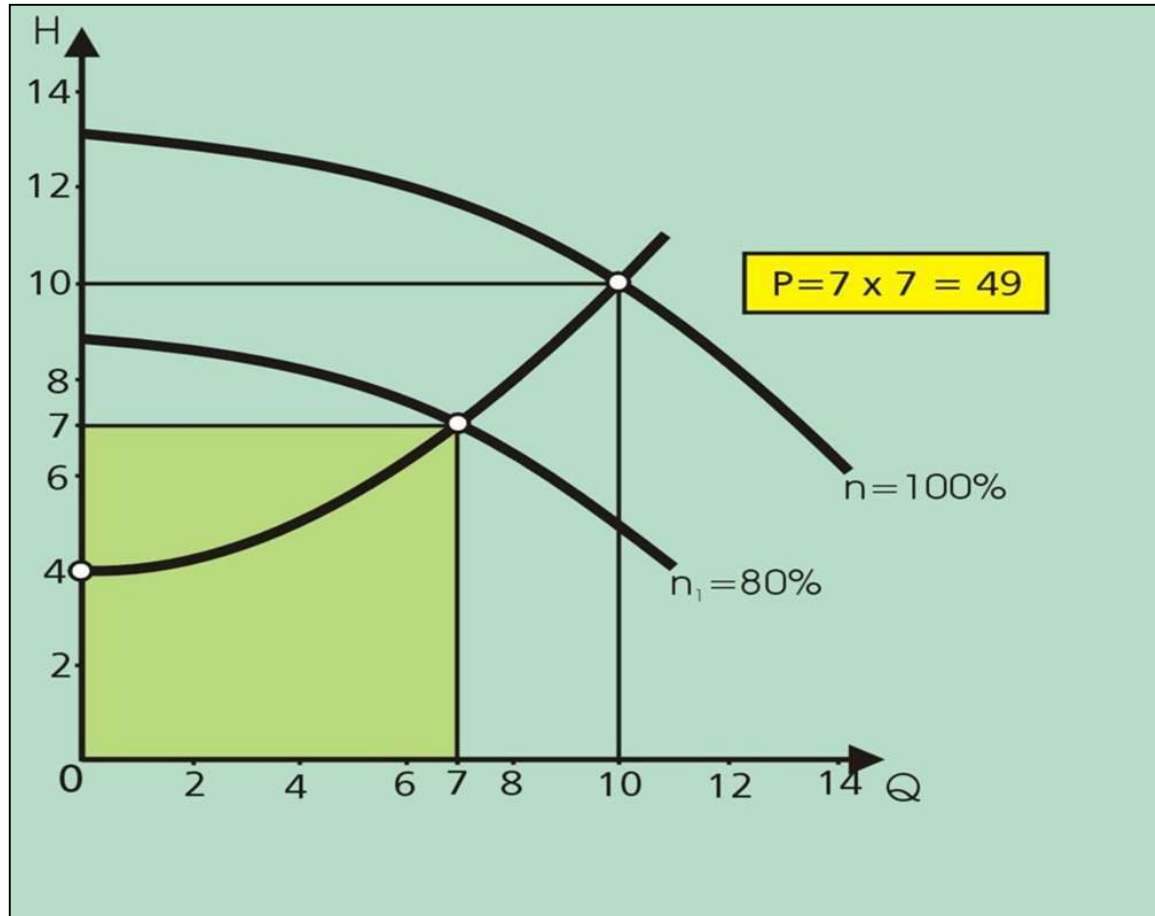
- Valve throttling increases system head resulting in excess power consumption
- Excess energy noted in blue area
- Excess energy impacts equipment reliability

# By-Passing



- Bypass lines require more flow, which results in excess power consumption.
- Excess energy impacts equipment reliability

# Variable Speed Control



- No excess energy used by the system
- Reliability is maximized



# Variable Speed Pumping

- Why use a variable speed pump?
- When to use variable speed?
- When not to use variable speed?

Source: Section supplied by Manitoba Hydro

# Change Pump Speed To Match Load

- Slower motor
- Two-speed motor\*
- Changes to belt drives/gears\*
- Variable Speed Drives
  - Variable Frequency Drive
  - Magnetic Drive
  - Fluid Drive

# Affinity Laws

• **Flow is Proportional to shaft speed**

$$(Q1/Q2) = (N1/N2)$$

**Pressure is Proportional to square of shaft speed**

$$(H1/H2) = (N1/N2)**2$$

**Power is Proportional to cube of shaft speed**

$$(P1/P2) = (N1/N2)**3$$

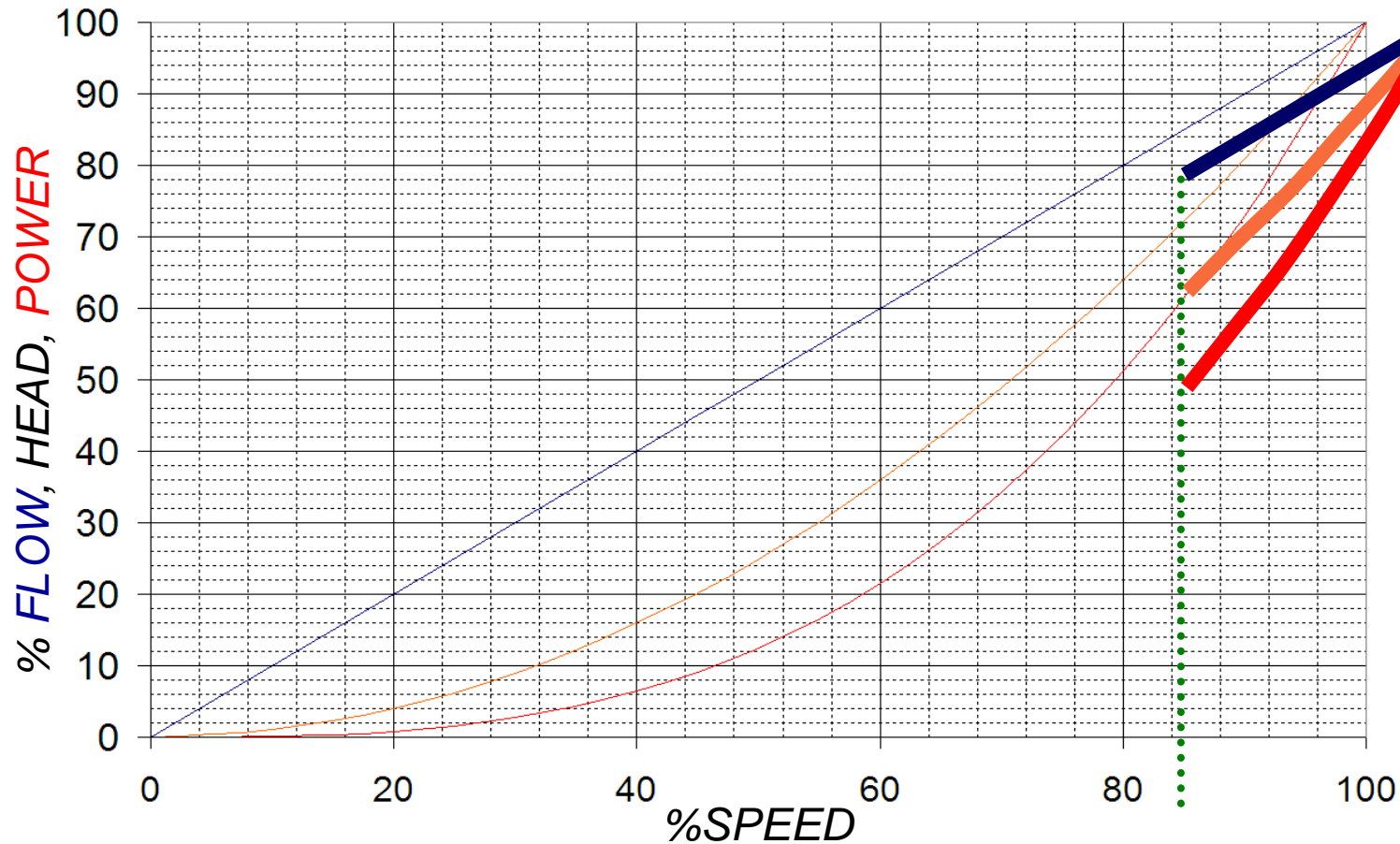
# Impact of Affinity Law

RPM	GPM	PSI	HP	% savings
3500	325	65	20	
3250	301.8	56.0	12.8	36%
3000	278.6	47.8	7.9	60%

**3000/3500 - 14% reduction = 60% HP reduction**

# Why use a Variable Speed Pump?

- Take advantage of the affinity rules of Centrifugal Pumps



# Traditional Flow Control

Most of the buildings in the 1970s used two basic types of flow control:

- flow bypasses, or
- throttling discharge valves with trimmed pump impellers.

Bypass arrangements is the least efficient and least used method of flow control.

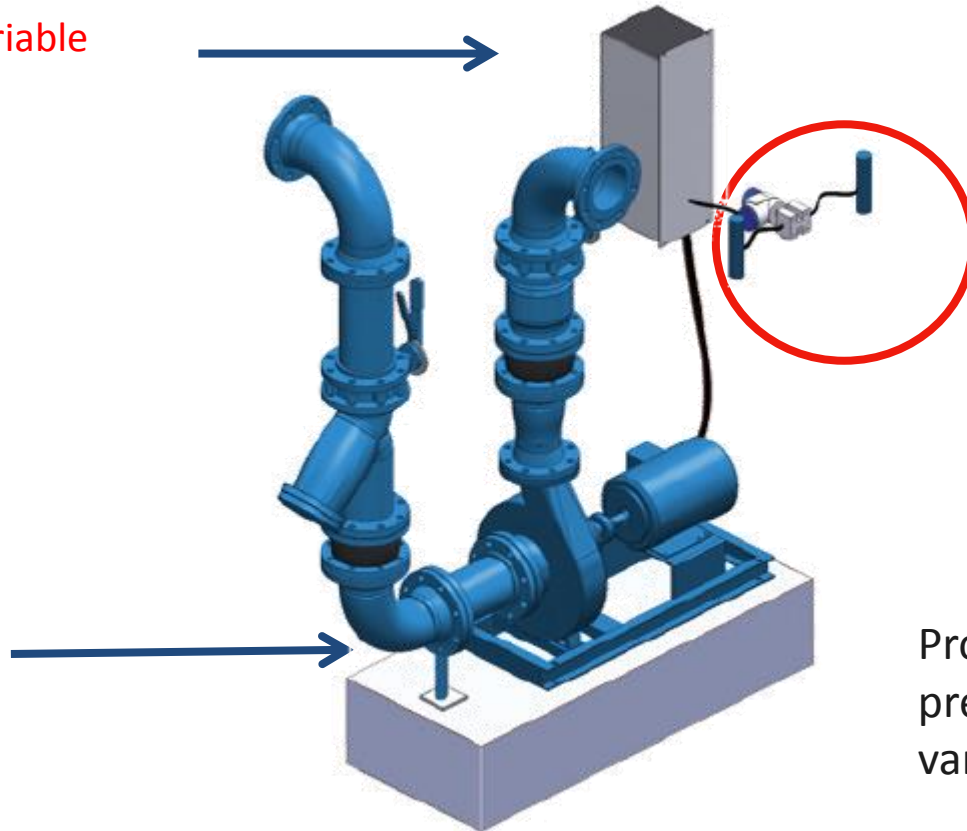
Throttling control does save energy compared to bypass methods; a variable speed operation can save much more energy.



# Traditional Variable Flow Systems with a DP Sensor

Wall-mounted Variable Frequency Drive

Horizontal Base Mounted Pump



Differential Pressure Sensor

Provides variable head pressure in a 2-way valve variable flow system

# Modern Control with Differential Pressure Sensor

The building industry has transitioned to using variable speed pumps with two-way valves to achieve variable flow.

Today, a system is composed of the pump, VFD, sensor, and two way valve to control HVAC systems.





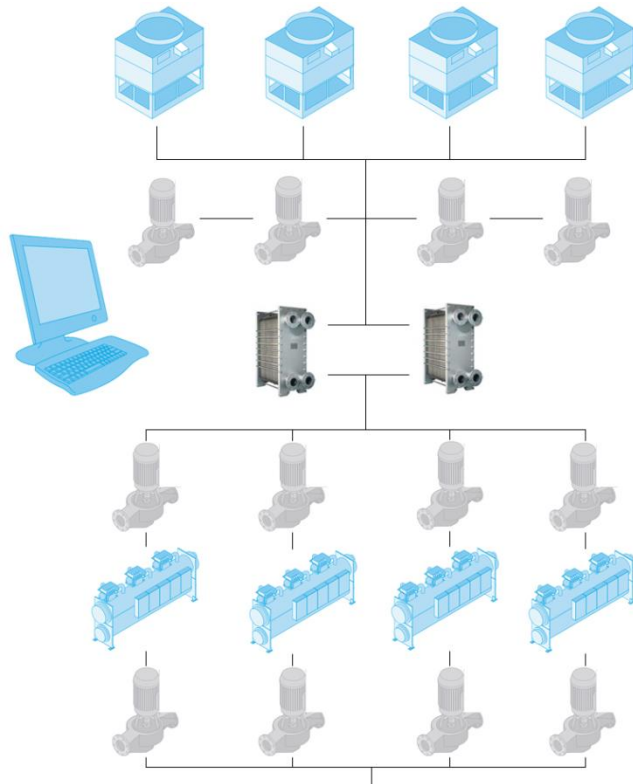
# Energy Metering Capability

The Variable Speed Drive can be used:  
As an energy meter for energy measurement verification, and  
For trending analysis towards demand response



# Traditional Chiller Plant Control Process Set-point Based

BMS



Automation  
Sequence

Parallel equipment  
staging (up/down)

Equipment  
speed control

Silo sub-system  
control

Traditional  
Logic

Capacity based  
sequencing

PID feedback  
control loops

Ambient reset

# Integrated Plant Control

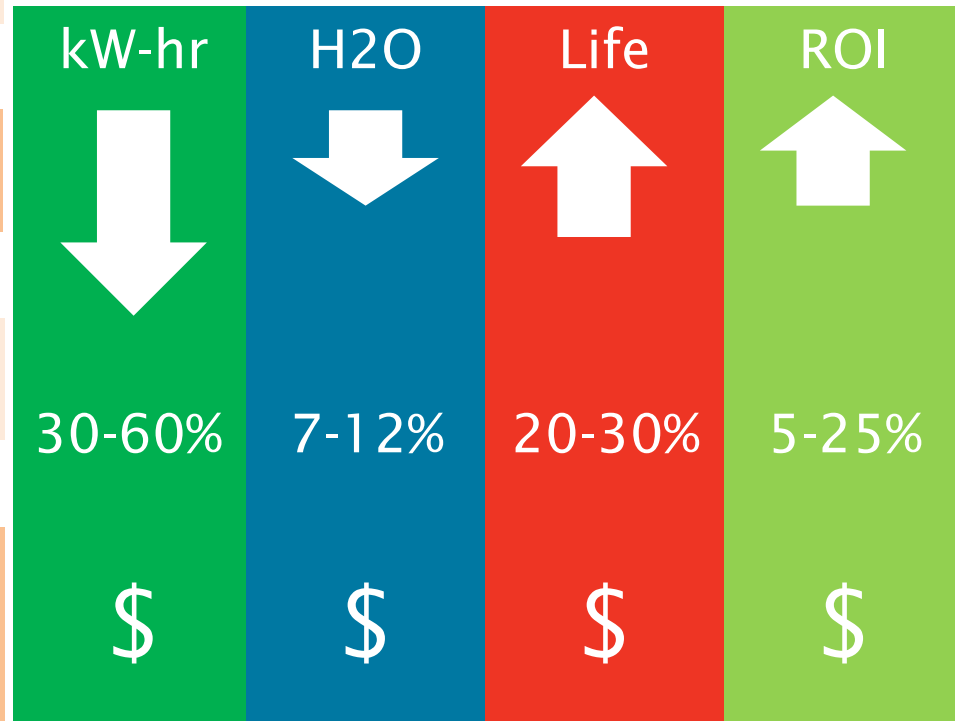
## Why Should You Be Interested?

Plant Annual energy Savings of **30-60%**

Annual Water Savings on the Cooling Tower of **7-12%**

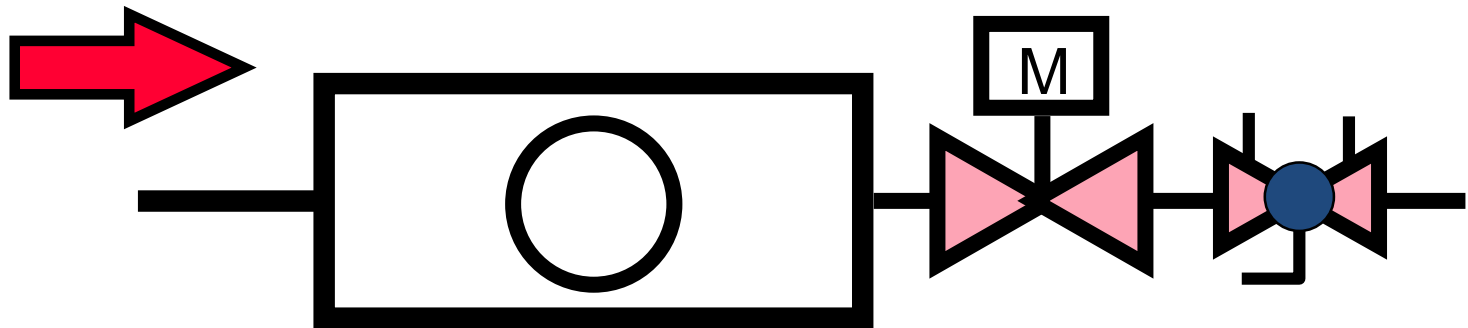
Longer Plant Equipment Life, **20-30%**

Protect your ROI with ECO\*PULSE On-board Diagnostic Service saving **5-25%** annual energy costs

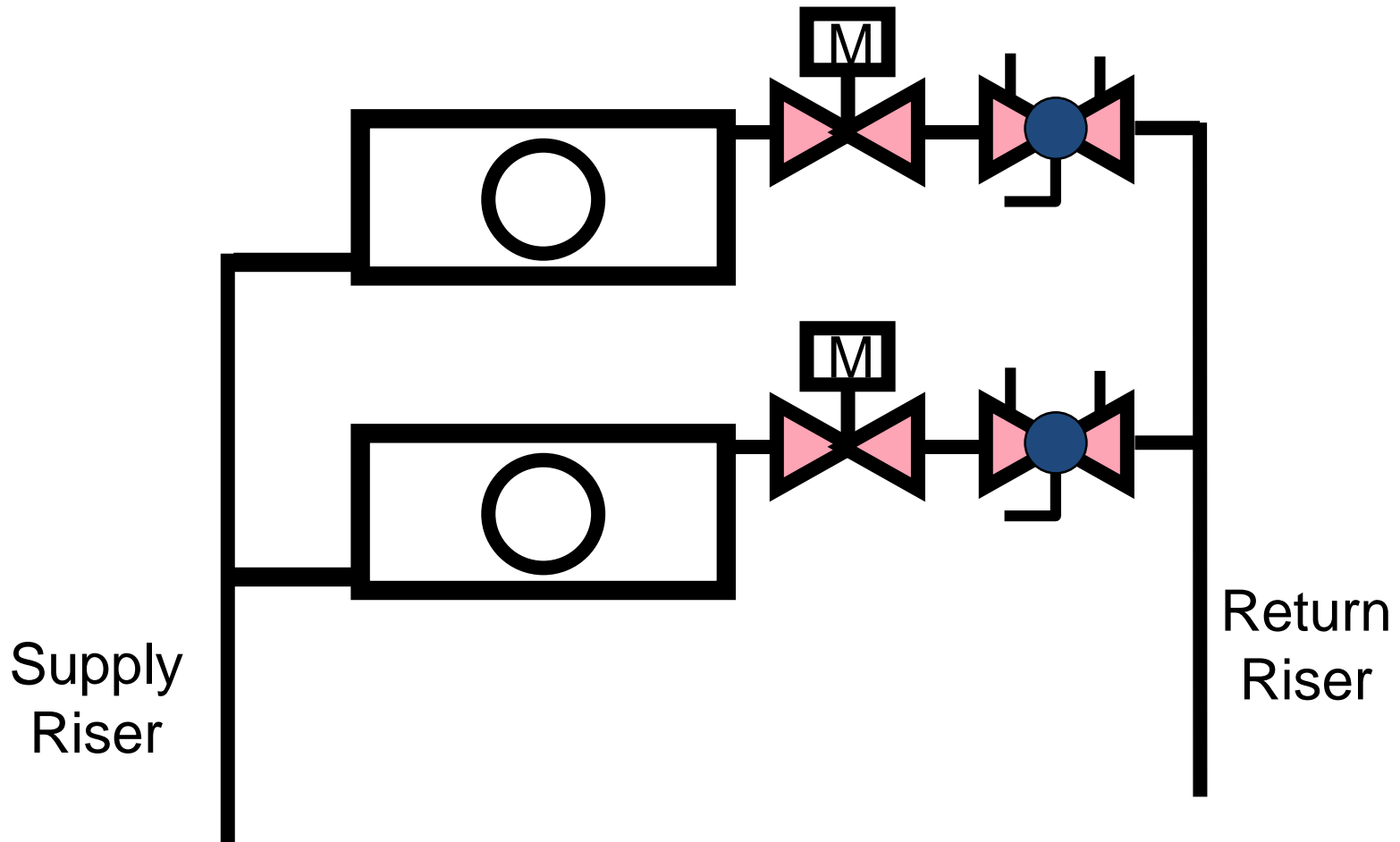


# Two-Way Valve Control

- Variable Flow Through Coil
- Variable Flow Through System



# Two-Way Valve Balance





# Control Valve Characteristics

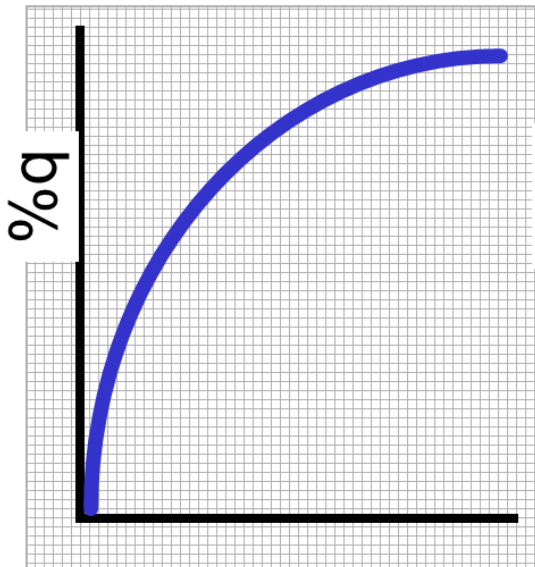
Coil  
Characteristic



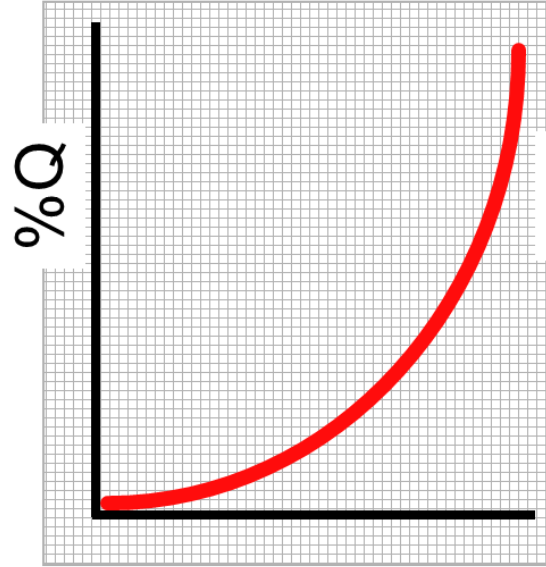
Valve  
Characteristic



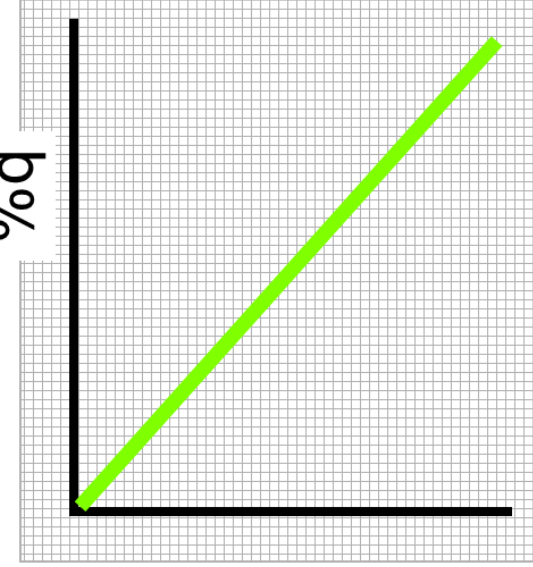
Combined  
Characteristic



% Flow

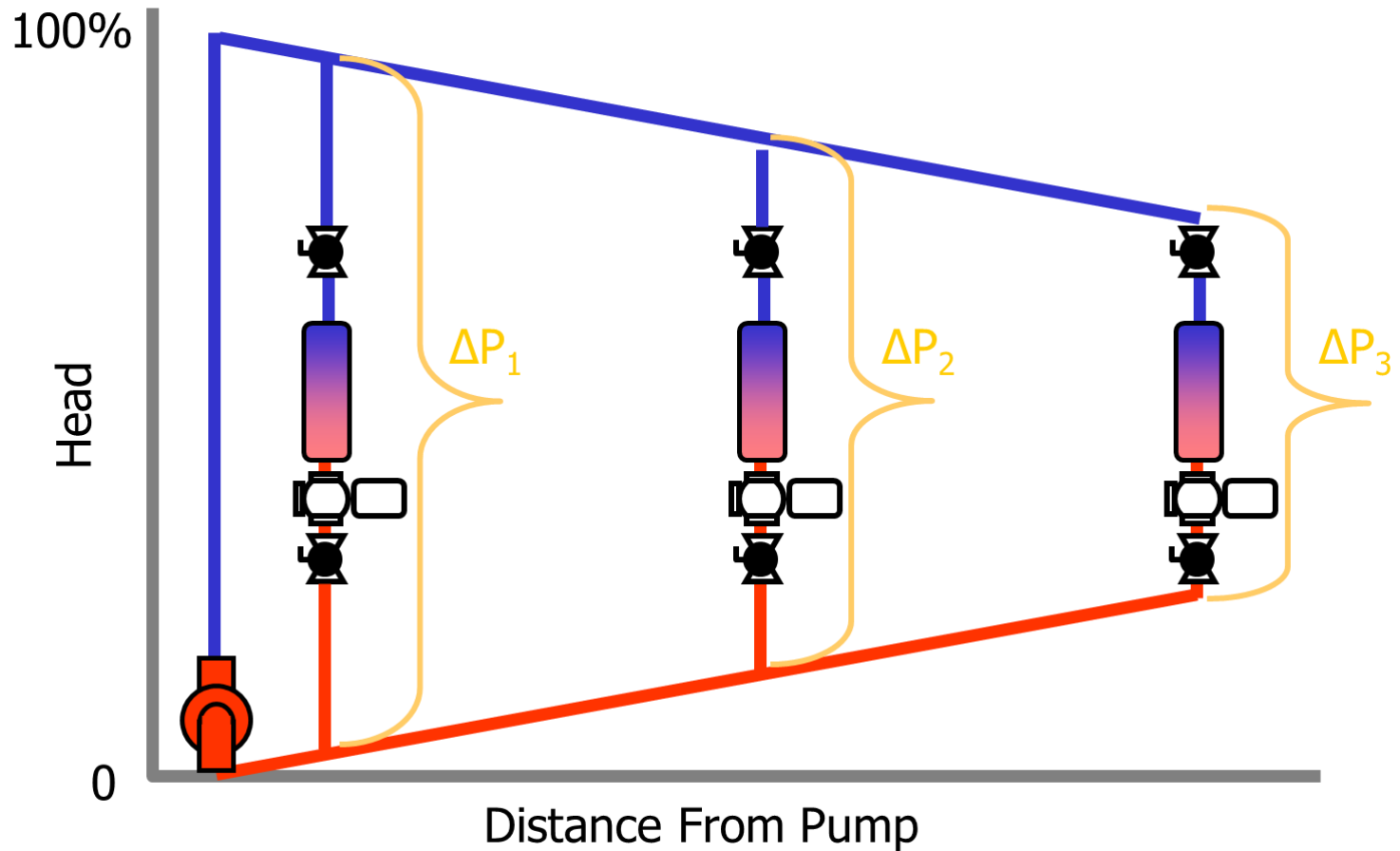


% Lift / Controller Output



% Control Output

# Why Balance? Two-Pipe Direct Return Has Unequal Branch Differential Pressures





# Flow Is Proportional To $\Delta P$

If all branches require the same design pressure drop:

- Branch 1 gets more flow than 2 or 3
- Branch 2 or 3 may get less than design flow
- Design temperature drops aren't as predicted
- System will use more pumping horsepower (more flow)

# Balancing, The Obvious Answer

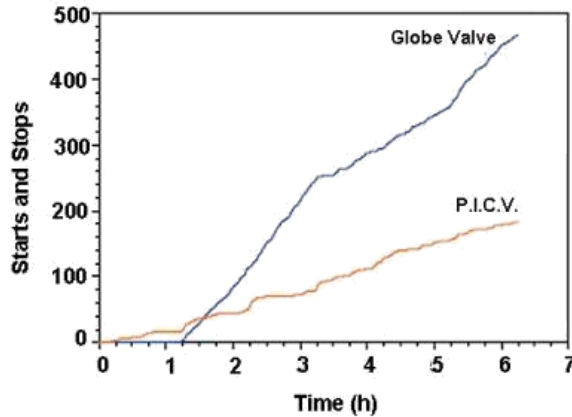
- Maximum branch flows need to be controlled
- Balancing valves are one solution
- Pressure independent flow control is another method
  - Prevents overflow conditions in branch

# Achieving Flow Control

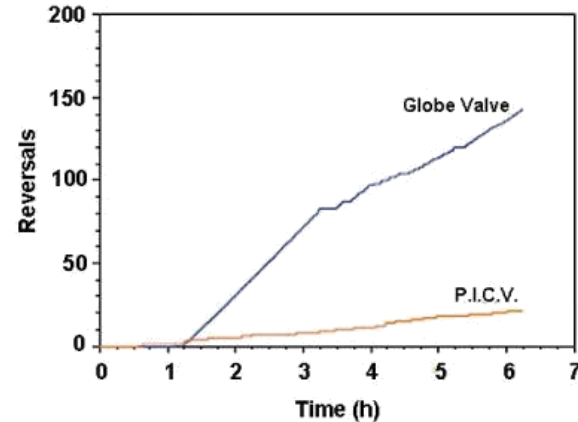
Two areas of concern:

1. Obtaining accurate, stable control of flow in the design range
  - Responsibility – Modulating temperature control valve
2. Preventing excess flow
  - Responsibility – balance device

# PICV vs Globe Valve in Operation (Pressure Independent Control Valve)

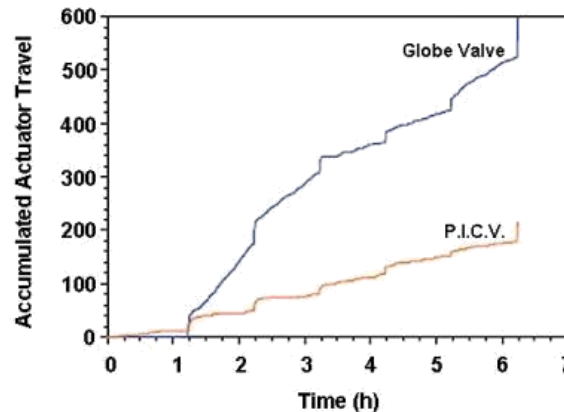


Accumulated Starts and Stops



Accumulated Actuator Reversals

Increased actuator travel and consequent over cooling/heating as the control valve hunts to find the right set point.



Accumulated Actuator Travel

# Benefits of PICV

- Pressure Independent Control Valves maintain 100% authority at all times
- Improve system efficiency
- Lower system energy cost
- Provide stable flow and higher  $\Delta T$
- An integrated solution - replaces balance and temperature control valves



# Takeaways

- **Source Equipment**
  - **Boilers – Condensing vs Non-condensing**
  - **Chillers – Centrifugal & Rotary Screw**
  - **Head Pressure Control**
- **Cooling Towers/Economizer**
  - **Good piping design**
  - **Integrated Waterside Economizer (Load Shaving)**
- **Expansion Tanks**
  - **Air Control vs Air Elimination**
  - **System pressure reference & PNPC**
  - **Cold fill pressure & thermal expansion**

# Takeaways

- Air Separators
  - Install at low pressure and high temperature
  - Centrifugal & coalescing air separators
- Heat Emitters (Fan coils, AHU)
  - Coil characteristic curves
- Control Valves
  - Pressure Dependent vs Pressure Independent
  - Inherent Characteristic
  - Branch Authority
- Balance Valves & Automatic Flow Limiters
  - Pressure Dependent vs Pressure Independent

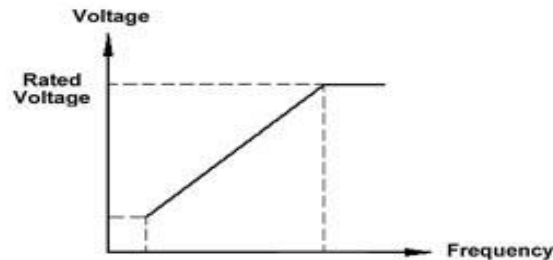
# Speed Range: Elements

- VFD's typically offer a frequency range of **0 to 60 Hz normal speed**. Most applications will only use a portion of the available frequency range.
- An application may only operate at one frequency, or it may operate throughout a **range** of frequencies, depending on process requirements.
- It is important to understand and define the range of variable speed required, as this may impact the **sizing** of VFD's and / or Motors.
- The Speed Range (turndown) of Pumps / Motors is usually specified as a **ratio** of nominal Motor synchronous speed to minimum speed.
- Basically simple division math
  - **2:1 (3600 – 1800 rpm), 4:1 (1800 to 450 rpm), 10:1 (3600 to 360 rpm), etc.**

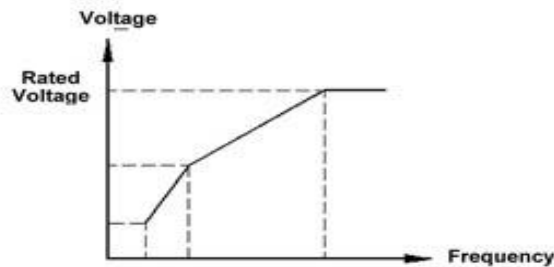


# Operating Principles

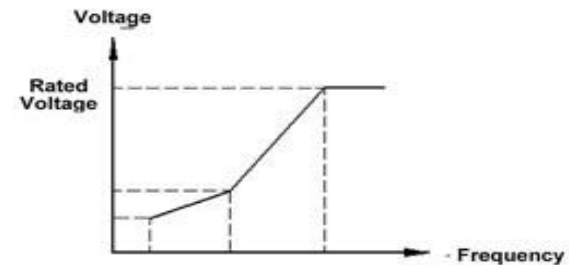
- When a VFD starts a motor, it initially applies a low frequency and voltage to the motor. The initial starting frequency is typically 2 Hz or less.
- The VFD will then **ramp up the output frequency and voltage** to a desired set point.



[Standard V/F Curve]



[When the startup torque is raised]



[When the startup torque is lowered]

# Typical VFD Features

- Adjustable electronic motor overload
- Instantaneous over-current / short circuit protection
- Ground fault (motor circuit)
- Under / over voltage protection
- Under current (no flow / dry run)
- Surge arrestors
- Forward / Reverse operation without the use of contactors
- Multiple Acceleration and Deceleration ramp rates
- Critical frequency avoidance (skip frequencies)
- Multiple stopping modes: Coast, Ramp or Dynamic Brake
- Process variable control
- Power Filters (DC-Chokes, EMI filter, Harmonic filters)
- Programmable Logic Controller

# Application Considerations for VFDs

- Pump selection and operating speed range:
  - Verify that the operating points throughout the speed range meet the desired head and flow conditions.
- Maximum and minimum speeds:
  - Verify that the pump and motor can safely operate at these speeds and meet the requirements of the application. For instance, flow or pressure requirements.
- Motor Selection considerations: (Consult the motor manufacturer)
  - Distance motor is located from frequency drive
  - Motor winding insulation class
  - Bearings type: standard versus insulated bearings
  - Protection: Temperature, vibration, shaft grounding brushes
  - Hazardous locations

# Application Considerations for VFDs

- Vibration:
  - Any critical / resonant frequencies to avoid
- Pump specific functions:
  - Cavitation protection, pipe fill, pipe burst, pipe blockage, deragging etc.
- Communication

# VFD Selection Considerations

## Voltage:

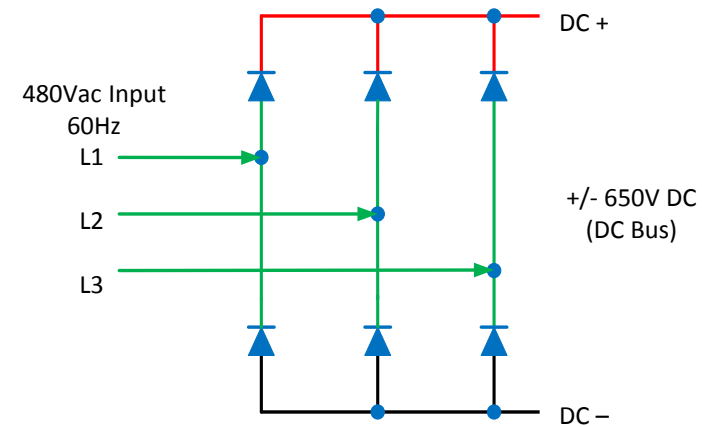
- What is the Voltage available on site?
- Does the VFD rated output V = Motor V?
- Single phase input?

## Amps:

- Motor Full Load Amps: Is the VFD output rating sufficient?
- Motor Service Factor Amps: Will the motor run into the SF?
- Load type: Variable Torque (110%) or Constant Torque (150%)?

## Environment:

- Temperature: Is Enclosure cooling or Heating needed?
- Ingress protection: Dust, moisture, corrosive gas?
- Elevation: More than 3,300ft above sea level?
- Hazardous location: Explosion proof?



# VFD Selection Considerations

## Motor cable length

- VFD output filters – to protect motors or to avoid nuisance tripping issues:
  - Output sine wave filters
  - dV/dt Filters
  - Common mode filters
- Consider the motor, pump, and drive as a complete system.

## Power Source Harmonic level: IEEE 519

- Line reactors
- DC Link chokes
- Active or Passive Harmonic Filter
- 12, 18 or 24 pulse rectifier VFD
- Active front end VFD



# VFD Selection Considerations

- Motor FLA amps are best (HP is not as accurate)
- Line Voltage & Phase (480v 3-phase or 230v single)
- Connected load type: Constant Torque / Variable Torque
- Enclosure requirements (NEMA 1, 12, 3R, 4 etc.)
- Motor Nameplate Data (full load current, rpm, etc.)
- Is motor insulation class 1000v or 1600v rated?
- Manual & automatic control signals
- Speed range. Ex. 0-60hz vs over-speeding to 70hz
- Duty Cycle requirements

# Summary

- Pump systems are big energy users
- Follow the plan as outlined in this workshop
- Operating (energy) and maintenance comprise 83% of the Life Cycle Cost of a typical pump system
- Look beyond energy savings
- System assessment/optimization should focus on improving the reliability/efficiency of the system



Thank you for your attendance